

ORDERING INFORMATION

| Part Number* | Package | Top Marketing |
|--------------|---------|---------------|
| MP6924GS | SOIC-8 | See Below |

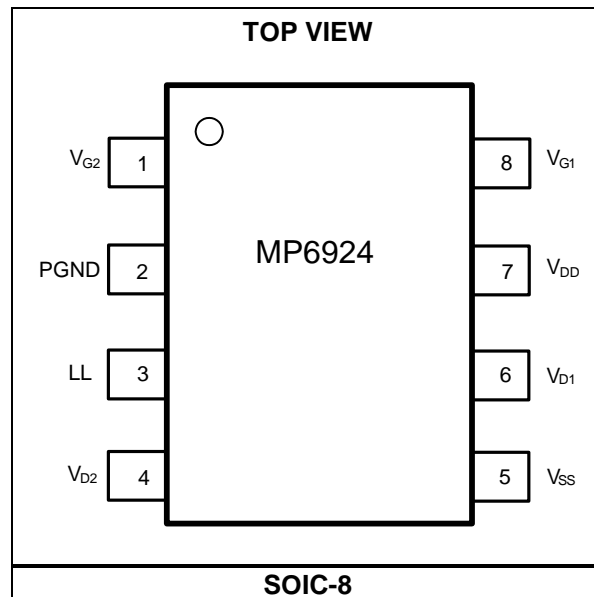
* For Tape & Reel, add suffix -Z (e.g. MP6924GS-Z)

TOP MARKING

MP6924
LLLLLLLL
MPSYWW

MP6924: Part number
 LLLLLLLL: Lot number
 MPS: MPS prefix
 Y: Year code
 WW: Week code

PACKAGE REFERENCE



ABSOLUTE MAXIMUM RATINGS ⁽¹⁾

| | |
|--|-----------------|
| V _{DD} to V _{SS} | -0.3V to +38V |
| PGND to V _{SS} | -0.3V to +0.3V |
| V _G to V _{SS} | -0.3V to +20V |
| V _D to V _{SS} | -1V to +180V |
| LL to V _{SS} | -0.3V to +6.5V |
| Continuous power dissipation (T _A = +25°C) ⁽²⁾ | |
| SOIC-8 | 1.4W |
| Junction temperature | 150°C |
| Lead temperature (solder) | 260°C |
| Storage temperature | -55°C to +150°C |

Recommended Operation Conditions ⁽³⁾

| | |
|---|-----------------|
| V _{DD} to V _{SS} | 4.2V to 35V |
| Operating junction temp. (T _J) .. | -40°C to +125°C |

Thermal Resistance ⁽⁴⁾

| | | |
|--------------|-----------------------|-----------------------|
| | θ_{JA} | θ_{JC} |
| SOIC-8 | 90 | 45 ... °C/W |

NOTES:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature T_J(MAX), the junction-to-ambient thermal resistance θ_{JA}, and the ambient temperature T_A. The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_D(MAX)=(T_J(MAX)-T_A)/θ_{JA}. Exceeding the maximum allowable power dissipation produces an excessive die temperature, causing the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) The device is not guaranteed to function outside of its operating conditions.
- 4) Measured on JESD51-7, 4-layer PCB.

ELECTRICAL CHARACTERISTICS

$V_{DD} = 12V$, $-40^{\circ}C \leq T_J \leq +125^{\circ}C$, unless otherwise noted.

| Parameter | Symbol | Conditions | Min | Typ | Max | Units |
|--|---------------|---|------|----------|------|-------------|
| V_{DD} voltage range | | | 4.2 | | 35 | V |
| V_{DD} UVLO rising | | | 3.7 | 3.95 | 4.2 | V |
| V_{DD} UVLO hysteresis | | | 0.13 | 0.185 | 0.24 | V |
| Operating current | I_{CC} | $C_{LOAD} = 4.7nF$, $F_{SW} = 100kHz$ | | 16 | 20 | mA |
| Quiescent current | I_Q | $V_{SS} - V_D = 0.5V$ | | 4.6 | 6 | mA |
| Shutdown current | | $V_{DD} = 4V$, $LL = 0V$ | | 135 | 190 | μA |
| | | $V_{DD} = 20V$, $LL = 0V$ | | 155 | 210 | |
| Light-load mode current | | | | 175 | 225 | μA |
| Thermal shutdown ⁽⁵⁾ | | | | 150 | | $^{\circ}C$ |
| Thermal shutdown hysteresis ⁽⁵⁾ | | | | 10 | | $^{\circ}C$ |
| Control Circuitry Section | | | | | | |
| $V_{SS} - V_D$ forward voltage | V_{fwd} | | 28 | 45 | 58 | mV |
| Turn off threshold ($V_{SS} - V_D$) | | | -56 | -40 | -20 | mV |
| Turn-on delay | t_{Don} | $C_{LOAD} = 4.7nF$, $V_{GS} = 2V$ | | 80 | 140 | ns |
| | t_{Don} | $C_{LOAD} = 10nF$, $V_{GS} = 2V$ | | 90 | 180 | ns |
| Input bias current on V_D | | $V_D = 180V$ | | | 1 | μA |
| Turn-on blanking time | t_{B_ON} | $C_{LOAD} = 4.7nF$ | 0.75 | 1.1 | 1.65 | μs |
| Turn-off blanking time ⁽⁵⁾ | t_{B_OFF} | $C_{LOAD} = 4.7nF$ | | 210 | | ns |
| Turn-off blanking V_{DS} threshold | V_{B_OFF} | | 1 | 1.7 | 2.5 | V |
| Light-load enter pulse width | T_{LL} | $R_{LL} = 100k\Omega$ | 1.7 | 2.3 | 3 | μs |
| Light-load turn-on pulse width hysteresis | T_{LL-H} | $R_{LL} = 100k\Omega$ | | 0.45 | | μs |
| Light-load enter delay | T_{LL-D} | | 0.5 | 1 | 1.52 | ms |
| Gate disable threshold on LL | V_{LL_DIS} | | 0.1 | 0.2 | 0.3 | V |
| Turn-on threshold (V_{DS}) | V_{LL_DS} | $V_{DD} = 12V$ | -330 | -230 | -130 | mV |
| Gate Driver Section | | | | | | |
| V_G (low) | V_{G_L} | $I_{LOAD} = 1mA$ | | | 0.1 | V |
| V_G (high) | V_{G_H} | $V_{DD} > 10V$ | | 11.5 | 13 | V |
| | | $V_{DD} \leq 10V$ | | V_{DD} | | |
| Turn-off propagation delay | | $V_D = V_{SS}$ | | | 55 | ns |
| Turn-off total delay | t_{Doff} | $V_D = V_{SS}$, $C_{LOAD} = 4.7nF$, $R_{GATE} = 0\Omega$, $V_{GS} = 2V$ | | 35 | 80 | ns |
| | t_{Doff} | $V_D = V_{SS}$, $C_{LOAD} = 10nF$, $R_{GATE} = 0\Omega$, $V_{GS} = 2V$ | | 45 | 100 | ns |
| Maximum source current ⁽⁶⁾ | | | | 0.5 | | A |
| Pull-down impedance | | | | 0.6 | 1.5 | Ω |

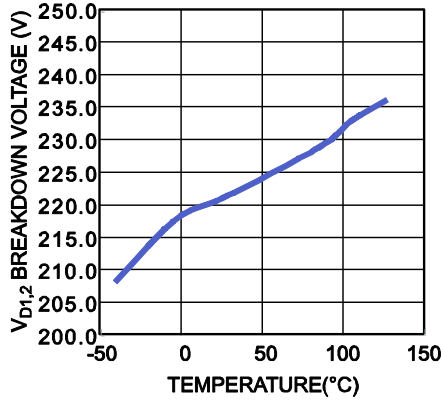
NOTES:

- 5) Guaranteed by characterization.
6) Guaranteed by design.

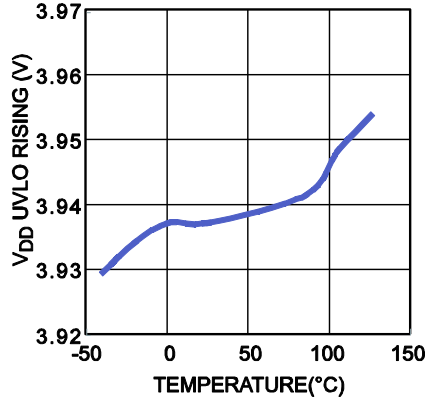
TYPICAL PERFORMANCE CHARACTERISTICS

$V_{DD} = 12V$, unless otherwise noted.

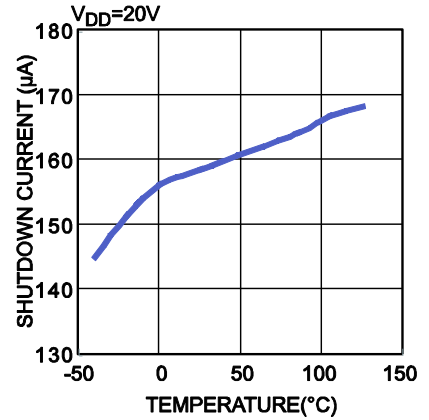
$V_{D1,2}$ Breakdown Voltage vs. Temperature



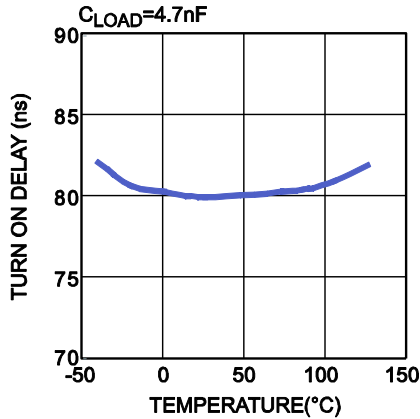
V_{DD} UVLO Rising vs. Temperature



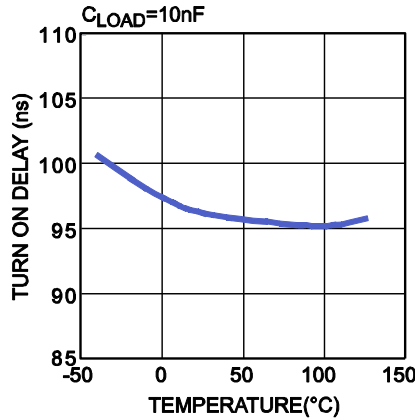
Shutdown Current vs. Temperature



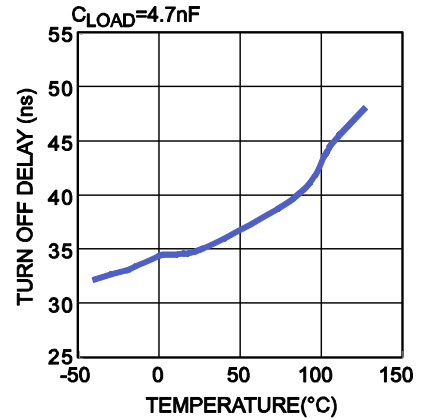
Turn-On Delay vs. Temperature



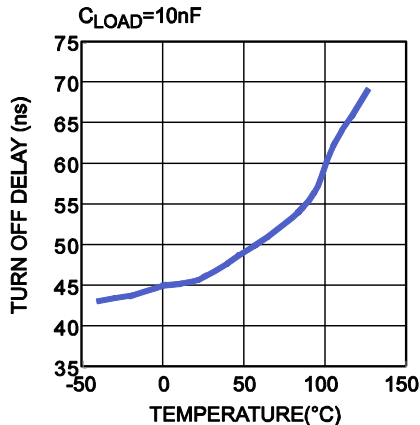
Turn-On Delay vs. Temperature



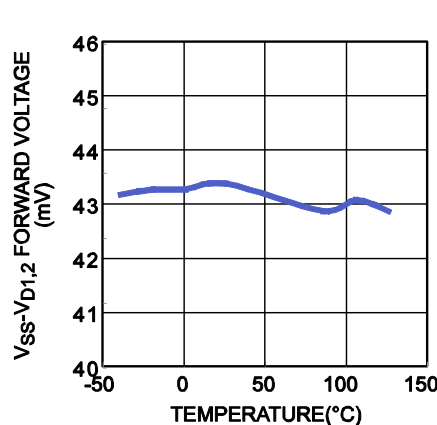
Turn-Off Delay vs. Temperature



Turn-Off Delay vs. Temperature



$V_{SS}-V_{D1,2}$ Forward Voltage vs. Temperature

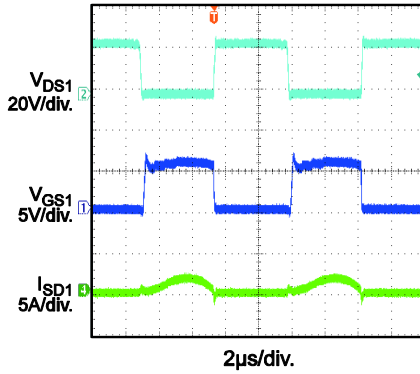


TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

$V_{DD} = 12V$, unless otherwise noted.

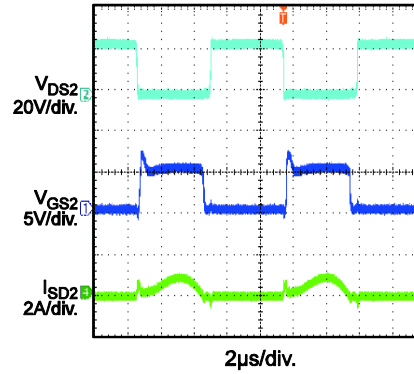
Operation in 90W LLC Converter

$V_{IN}=240VAC$, $V_{OUT}=12V$, $I_{OUT}=0.75A$



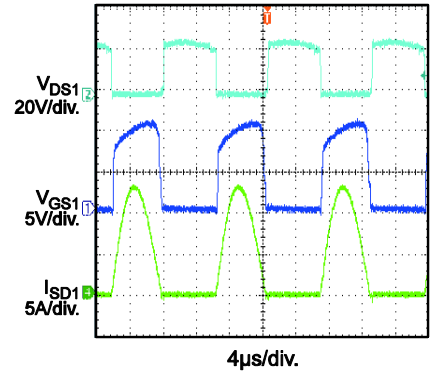
Operation in 90W LLC Converter

$V_{IN}=240VAC$, $V_{OUT}=12V$, $I_{OUT}=0.75A$



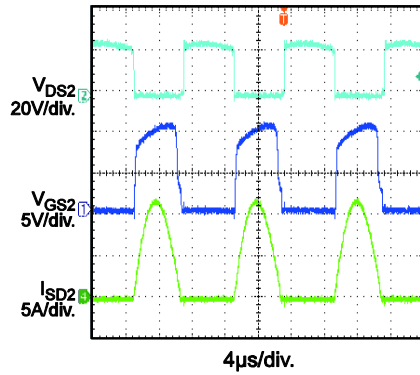
Operation in 90W LLC Converter

$V_{IN}=240VAC$, $V_{OUT}=12V$, $I_{OUT}=7.5A$



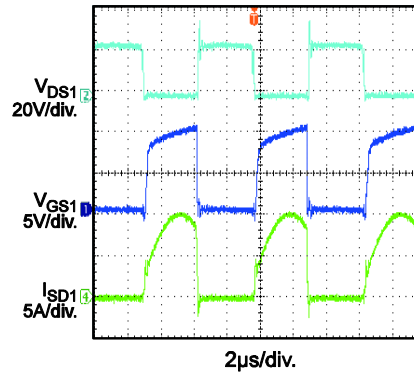
Operation in 90W LLC Converter

$V_{IN}=240VAC$, $V_{OUT}=12V$, $I_{OUT}=7.5A$



Operation in 90W LLC Converter

$V_{IN}=265VAC$, $V_{OUT}=12V$, $I_{OUT}=7.5A$



PIN FUNCTIONS

| Pin # (SOIC-8) | Name | Description |
|-------------------|----------|--|
| 1 | V_{G2} | MOSFET 2 gate driver output. |
| 2 | PGND | Power ground. PGND is the power switch return. |
| 3 | LL | Light-load timing setting. Connect a resistor to LL to set the light-load timing. Leave LL open to prevent the IC from entering light-load mode. Pull LL low to disable the gate driver. Connect a capacitor to LL to set the forward voltage drop. |
| 4 | V_{D2} | MOSFET 2 drain voltage sense. |
| 5 | V_{SS} | Source pin used as reference for V_{D1} and V_{D2}. |
| 6 | V_{D1} | MOSFET 1 drain voltage sense. |
| 7 | V_{DD} | Supply voltage. |
| 8 | V_{G1} | MOSFET 1 gate driver output. |

BLOCK DIAGRAM

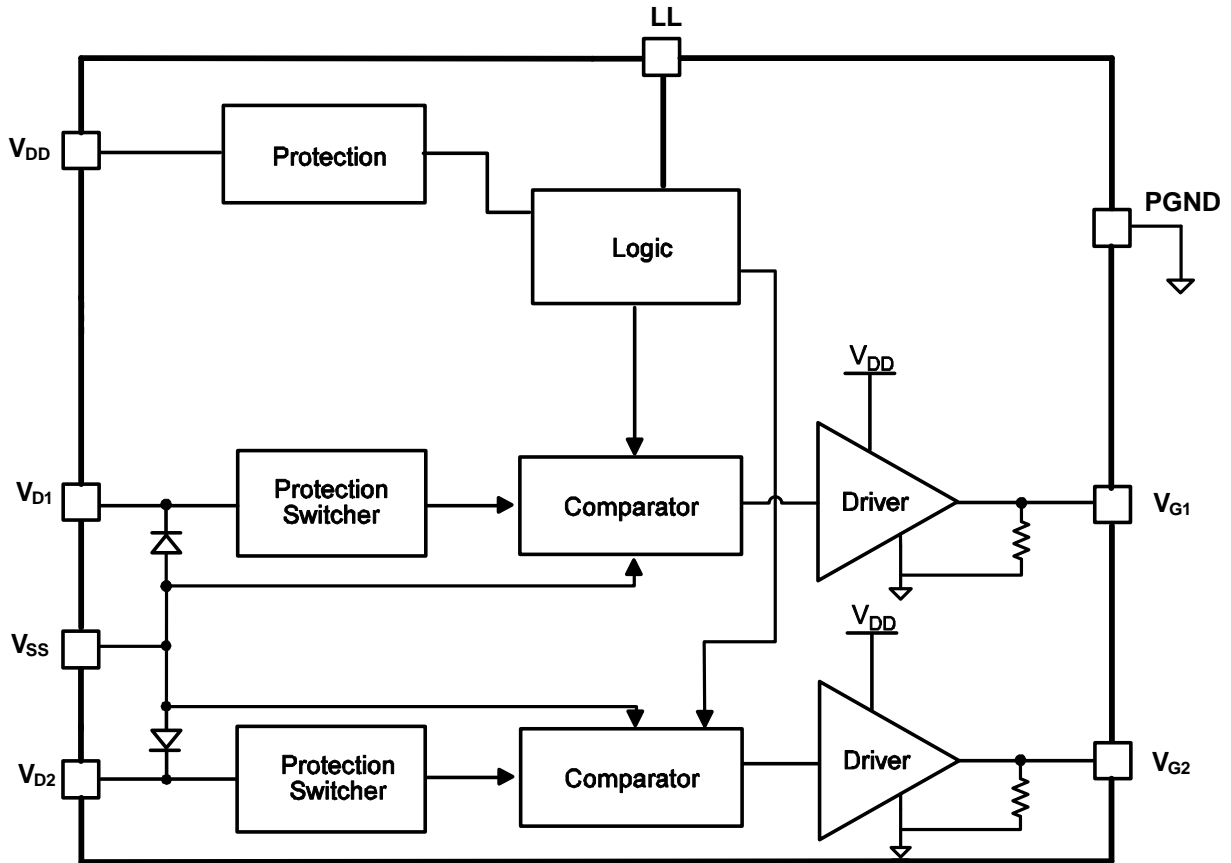


Figure 1: Functional Block Diagram

OPERATION

The MP6924 operates in discontinuous conduction mode (DCM), continuous conduction mode (CCM), and critical conduction mode (CrCM). When the MP6924 operates in either DCM or CrCM, the control circuitry controls the gate in forward mode, and the gate turns off when the MOSFET current is low. In CCM, the control circuitry turns off the gate during very fast transients.

VD Clamp

Because $V_{D1,2}$ can go as high as 180V, a high-voltage JFET is used at the input. To prevent excessive currents when $V_{G1,2}$ goes below $-0.7V$, a $1k\Omega$ resistor is recommended between $V_{D1,2}$ and the drain of the external MOSFET.

Under-Voltage Lockout (UVLO)

When V_{DD} is below the V_{DD} UVLO threshold, the MP6924 falls into sleep mode and $V_{G1,2}$ remains at a low level.

Enable

If LL is pulled low, the MP6924 is in shutdown mode, which consumes $175\mu A$ of shutdown current. If LL is pulled high during the rectification cycle, the gate driver will not appear until the next rectification cycle begins (see Figure 2).

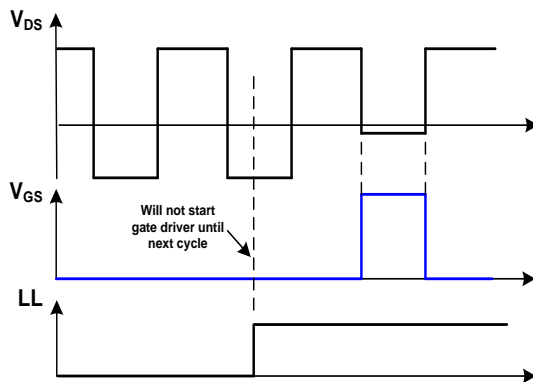


Figure 2: LL Control Scheme

Thermal Shutdown

If the junction temperature of the chip exceeds $150^{\circ}C$, $V_{G1,2}$ is pulled low, and the MP6924 stops switching. The MP6924 resumes normal function after the junction temperature drops to $140^{\circ}C$.

Turn-On Phase

When the switch current flows through the body diode of the MOSFET, there is a negative voltage drop ($V_D - V_{SS}$) across the body diode. V_{DS} is much lower than the turn-on threshold of the control circuitry (V_{LL-DS}), which triggers a maximum 500mA of charge current to turn on the MOSFET (see Figure 3).

Turn-On Blanking

The control circuitry contains a blanking function that ensures that when the MOSFET turns on or off, it remains in that state for t_{B_ON} ($\sim 1.1\mu s$), which determines the minimum on time. During the turn-on blanking period, the turn-off threshold is not blanked completely, but changes to about $+100mV$ (instead of $+40mV$). This ensures that the part can always turn off, even during the turn-on blanking period, although it does so slower. Avoid setting the synchronous period below t_{B_ON} in CCM condition in the LLC converter to eliminate shoot-through.

Conduction Phase

When V_{DS} rises above the forward voltage drop ($-V_{fwd}$) according to the decrease of the switching current, the MP6924 pulls down the gate voltage level to make the on resistance of the synchronous MOSFET larger to ease the rise of V_{DS} .

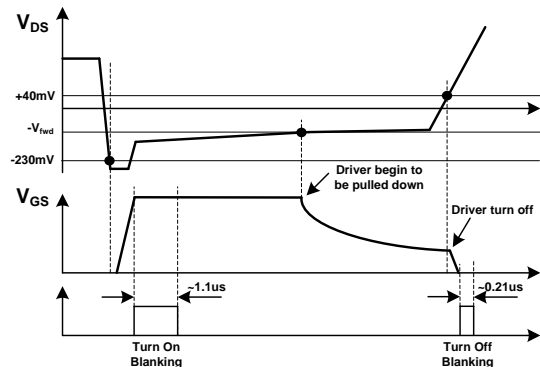


Figure 3: Turn-On/Off Timing Diagram

The control scheme in Figure 3 shows V_{DS} adjusted to be around $-V_{fwd}$, even when the current through the MOSFET is fairly low. This function puts the driver voltage at a very low level when the synchronous MOSFET is turning off, which boosts the turn-off speed. V_{fwd} can be programmable on LL.

Turn-Off Phase

When V_{DS} rises to trigger the turn-off threshold (+40mV), the gate voltage is pulled to zero after a very short turn-off delay (see Figure 3).

Turn-Off Blanking

After the gate driver is pulled to zero by V_{DS} reaching the turn-off threshold (+40mV), turn-off blanking is triggered to ensure that the gate driver is off for at least 210ns to prevent an error trigger on V_{DS} .

Light-Load Latch-Off Function

The gate driver of the MP6924 is latched off to save driver loss in light-load condition and improve efficiency.

When the MOSFET's switching cycle conducting period falls below $2.3\mu\text{s}$ (T_{LL}), the MP6924 enters light-load mode and latches off the MOSFET after a 1ms delay (light-load enter delay, T_{LL-D}) (see Figure 4).

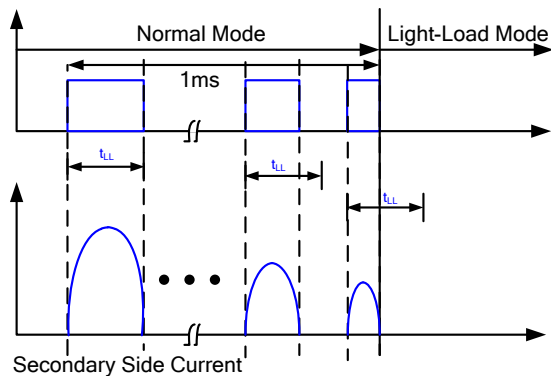


Figure 4: MP6924 Entering Light-Load Mode

During light-load mode, the MP6924 monitors the body diode conduction time. If this time exceeds $2.75\mu\text{s}$ ($T_{LL} + T_{LL-H}$), the IC exits light-load mode and initiates the gate driver in the next new switching cycle (see Figure 5 and Figure 6).

Light-load enter timing (T_{LL}) is programmable by connecting a resistor (R_{LL}) to LL. By monitoring the LL current (the LL voltage is kept at $\sim 2\text{V}$ internally), T_{LL} can be calculated with Equation (1):

$$T_{LL} = R_{LL} (\text{k}\Omega) \cdot \frac{2.3\mu\text{s}}{100\text{k}\Omega} \quad (1)$$

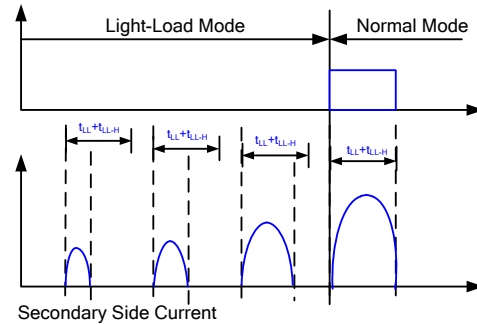


Figure 5: MP6924 Exiting Light-Load Mode

If the light-load mode of the MP6924 ends during the rectification cycle, the gate driver signal does not appear until the next rectification cycle starts (see Figure 6).

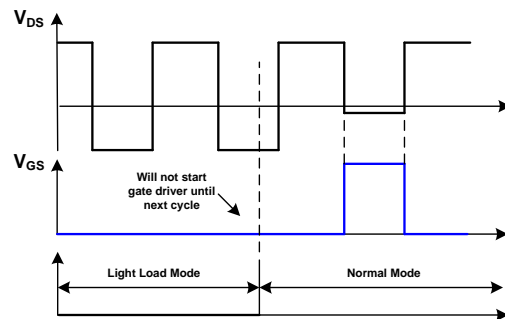


Figure 6: Gate Driver Starts After Exiting Light-Load Mode

Anti-Bounce Logic

The MP6924 has anti-bounce logic, which helps protect the two-channel driver against cross conduction.

Figure 7 shows the anti-bounce logic for the two-channel driver. When channel 1 or 2 are turned off, the corresponding channel gate driver is blanked until another channel is switched off.

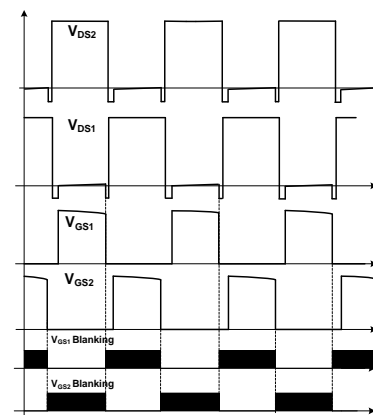


Figure 7: Anti-Bounce Logic of the Gate Driver

APPLICATION INFORMATION

Layout Considerations

Listed below are the main recommendations that should be taken into consideration when designing the PCB.

Sensing for V_D/V_S

1. Keep the sensing connections (V_{D1}/V_{SS} , V_{D2}/V_{SS}) as close to each of the MOSFETs (drain/source) as possible.
2. Keep the two channels' sensing loops separated from each other.
3. Make the sensing loop as small as possible (see Figure 8).

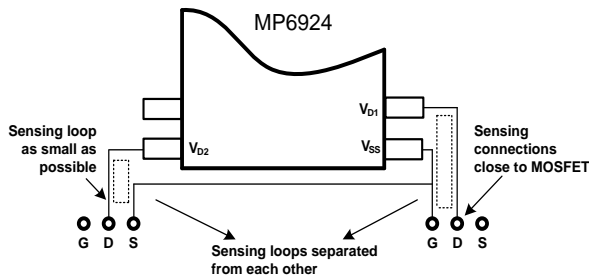


Figure 8: Sensing for V_D/V_S

Figure 9 shows a layout example of the MP6924 driving PowerPAK SO8 package MOSFETs with two, separate, small sensing loops.

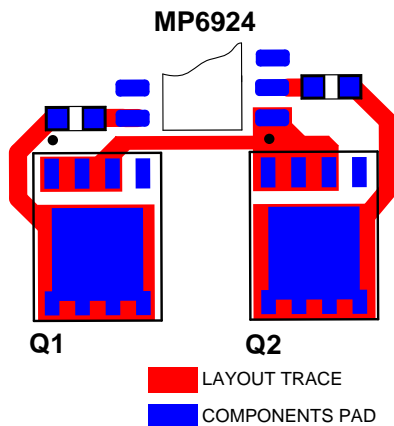


Figure 9: Layout Example for Sensing Loop and V_{DD} Decoupling

V_{DD} Decoupling Capacitor

1. Place a decoupling capacitor no smaller than $1\mu\text{F}$ from V_{DD} to PGND close to the IC for adequate filtering (see Figure 10).

System Power Loop

1. Keep the two channels' power loops separated from each other (see Figure 10).
This minimizes the interaction between the two channels' power loops, which may affect the voltage sensing of the IC.
2. Make the power loop as small as possible to reduce parasitic inductance.

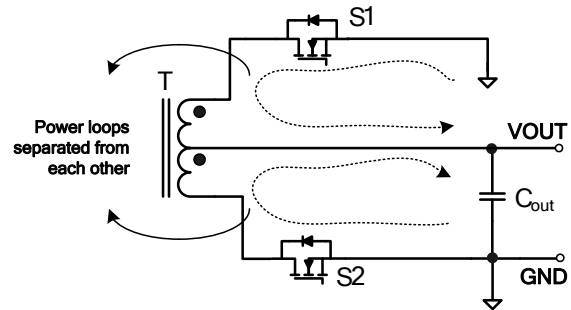


Figure 10: System Power Loop

Figure 11 shows a layout example of the power loop trace, which has a minimized loop length. The two channel power traces do not cross each other.

It is highly recommended to place the driver's sensing loop trace away from the power loop trace (see Figure 11). The sensing loop trace and power loop trace can be placed on different layers to keep them separate from each other.

Do not place the driver IC inside the power loop; this may affect MOSFET voltage sensing.

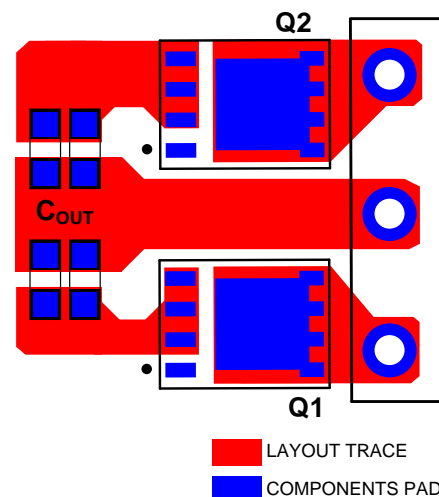


Figure 11: Layout Example for System Power Loop

SR MOSFET Selection and Driver Ability

Power MOSFET selection is a trade-off between $R_{DS(ON)}$ and Q_g . To achieve high efficiency, a MOSFET with a smaller $R_{DS(ON)}$ is recommended. A larger Q_g with a smaller $R_{DS(ON)}$ makes the turn-on/off speed lower and the power loss larger. For the MP6924, V_{DS} is adjusted at V_{fwd} during the driving period. A MOSFET with a small $R_{DS(ON)}$ is not recommended because the gate driver may be kept at a fairly low level with a small $R_{DS(ON)}$, even when the system load is high, which makes the advantage of the low $R_{DS(ON)}$ inconspicuous.

Figure 12 shows the typical waveform of the LLC on the secondary side. To achieve a fairly high usage of the MOSFET's $R_{DS(ON)}$, it is expected that the MOSFET driver voltage is kept at the maximum level until the last 25% of the SR conduction period. Calculate V_{DS} with Equation (2):

$$V_{DS} = -R_{ds(ON)} \cdot \frac{\sqrt{2}}{2} \cdot I_{peak} = -R_{ds(ON)} \cdot I_{OUT} = -45mV \quad (2)$$

Where V_{DS} is drain-source voltage of the MOSFET.

The MOSFET's $R_{DS(ON)}$ is recommended to be no lower than $\sim V_{fwd}/I_{OUT}$ (m Ω). For example, in a 10A application with V_{fwd} at 45mV, the $R_{DS(ON)}$ of the MOSFET is recommended to be no lower than 4.5m Ω .

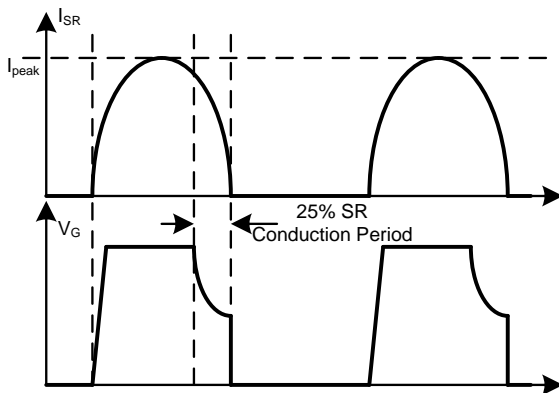


Figure 12: Synchronous Rectification Typical Waveform in LLC

Q_g of the MOSFET affects the turn-on and turn-off delay. Figure 3 indicates the turn-on delay (t_{Don}) and the turn-off delay (t_{Doff}). t_{Don} indicates how long the body diode conducts before the MOSFET is turned on, while t_{Doff} indicates how long the driver takes to turn off the MOSFET. With a higher turn-on delay, the body diode conduction duration of the MOSFET is longer, which brings down the total efficiency. However, with a higher turn-off delay, the shoot-through risk is higher in CCM operation.

Figure 13 and Figure 14 show the t_{Don} and t_{Doff} of the MP6924 according to different C_{load} values.

Turn-On Delay vs. C_{LOAD}

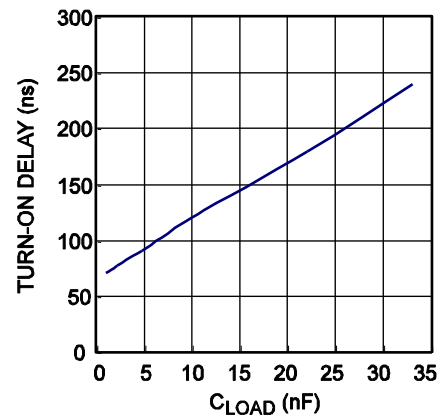


Figure 13: Turn-On Delay vs. C_{load}

Turn-Off Delay vs. C_{LOAD}

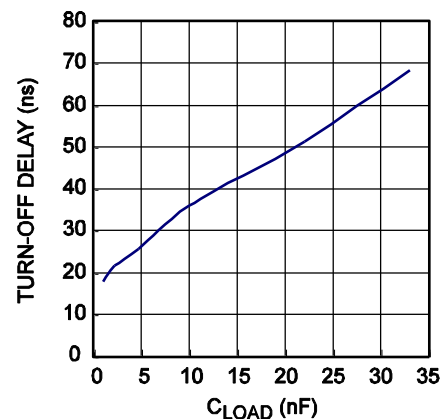


Figure 14: Turn-Off Delay vs. C_{load}

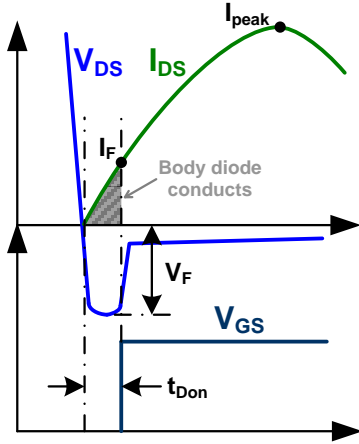


Figure 15: Turn-On Delay Effect on Efficiency

Figure 15 shows how t_{Don} affects system efficiency. During t_{Don} , the body diode of the SR MOSFET conducts, which leads to a power loss that can be calculated with Equation (3):

$$P_{on} \approx \frac{V_F \cdot I_F}{2} \cdot 2f_s \cdot t_{Don} = V_F \cdot I_F \cdot f_s \cdot t_{Don} \quad (3)$$

Where V_F is the body diode forward voltage drop, I_F is the switching current when the turn-on delay (t_{Don}) has ended, and f_s is the switching frequency.

When considering the switching current as a complete sine wave, I_F can be estimated with Equation (4) and Equation (5):

$$I_F = I_{peak} \cdot \sin(2 \cdot f_s \cdot t_{Don} \cdot \pi) \quad (4)$$

$$I_{peak} \approx \frac{\pi}{2} \cdot I_{out} \quad (5)$$

Where I_{peak} is the peak switching current through the MOSFET, and I_{out} is the system output current.

When plugging the values from Equation (4) and Equation (5) into Equation (3), the turn-on delay power loss through the SR MOSFET's body diode can be derived with Equation (6):

$$P_{on} = \frac{\pi}{2} \cdot I_{out} \cdot V_F \cdot f_s \cdot t_{Don} \cdot \sin(2 \cdot f_s \cdot t_{Don} \cdot \pi) \quad (6)$$

Figure 14 shows how different turn-on delay values affect efficiency according to different output voltages. To keep the body diode conduction loss at a fairly low level (below 0.5% of the output power), the turn-on delay is recommended to be less than 5% of the switching cycle. For example, in a $f_{sw} = 200\text{kHz}$ LLC system, the switching cycle is $\sim 5\mu\text{s}$, and it is recommended to select the MOSFET to make $t_{Don} < 250\text{ns}$.

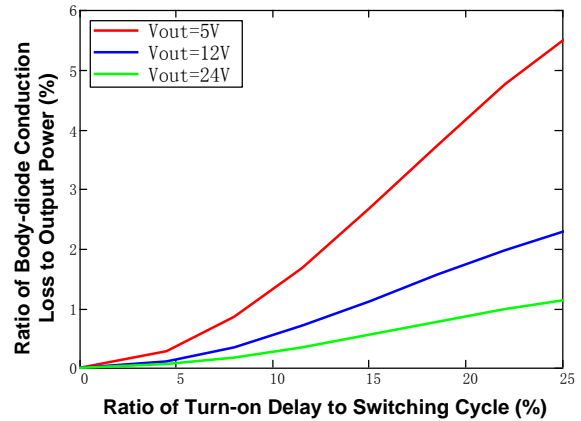
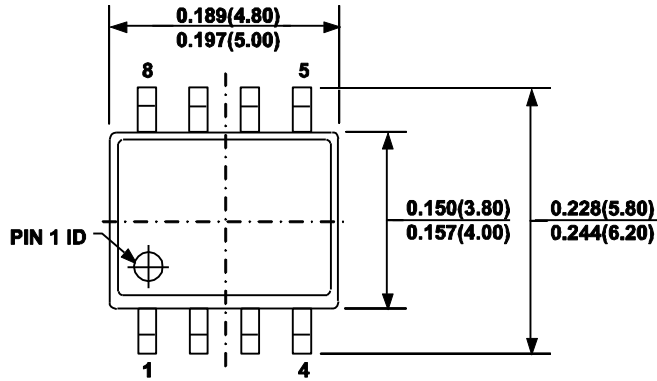


Figure 14: Turn-On Delay vs. Power Loss

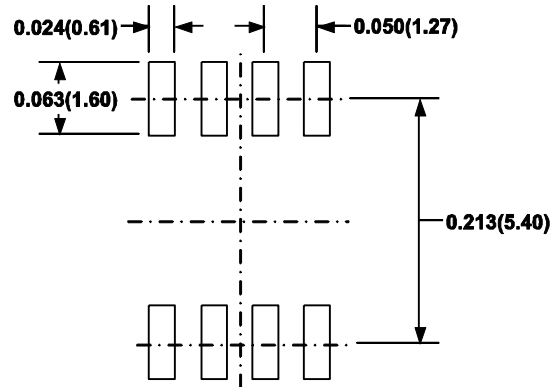
The turn-off delay (t_{Doff}) is critical in some fast transient CCM applications. Choose the MOSFET to make t_{Doff} below the CCM current transient duration. Otherwise, the MOSFET may need to be selected with a lower Q_g , or an external totem pole driver circuit may be added to prevent shoot-through.

PACKAGE INFORMATION

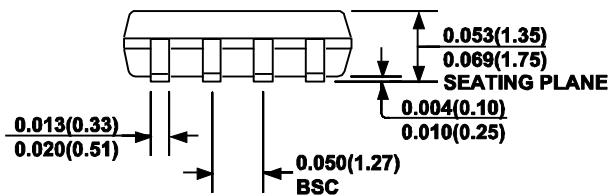
SOIC-8



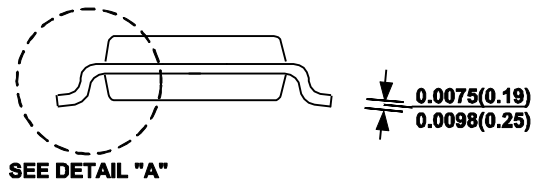
TOP VIEW



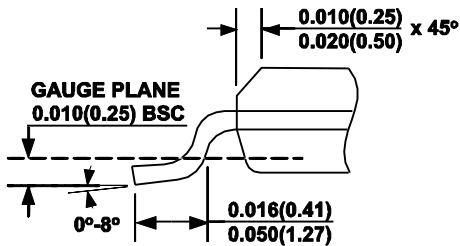
RECOMMENDED LAND PATTERN



FRONT VIEW



SIDE VIEW



DETAIL "A"

NOTE:

- 1) CONTROL DIMENSION IS IN INCHES. DIMENSION IN BRACKET IS IN MILLIMETERS.
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.
- 4) LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.004" INCHES MAX.
- 5) DRAWING CONFORMS TO JEDEC MS-012, VARIATION AA.
- 6) DRAWING IS NOT TO SCALE.

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