ISL78692

Li-ion/Li-Polymer Battery Charger

FN8692
Rev.1.00
Mar 29, 2017

The ISL78692 is an integrated single-cell Li-ion or Li-polymer battery charger capable of operating with an input voltage as low as 2.65V (cold crank case). This charger is designed to work with various types of AC adapters or a USB port.

The ISL78692 operates as a linear charger when the AC adapter is a voltage source. The battery is charged in a CC/CV (constant current/constant voltage) profile. The charge current is programmable with an external resistor up to 1A. The ISL78692 can also work with a current-limited adapter to minimize the thermal dissipation.

The ISL78692 features charge current thermal foldback to guarantee safe operation when the printed circuit board's thermal dissipation is limited due to space constraints. Additional features include preconditioning of an over-discharged battery, an NTC thermistor interface for charging the battery in a safe temperature range and automatic recharge. The device is specified for operation in ambient temperatures from -40°C to +85°C and is offered in a 3x3mm thermally enhanced DFN package.

Related Literature

- Technical Brief TB363 "Guidelines for Handling and Processing Moisture Sensitive Surface Mount Devices (SMDs)"
- Technical Brief TB379 "Thermal Characterization of Packaged Semiconductor Devices"
- UG001, "ISL78692EVAL1Z Evaluation Board User Guide"

Features

- Complete charger for single-cell Lithium chemistry batteries
- Integrated power transistor and current sensor
- Reverse battery leakage 700nA
- 1% initial voltage accuracy
- Programmable CC current up to 1A
- Charge current thermal foldback
- NTC thermistor interface for battery temperature alert
- Accepts CV and CC types of adapters or USB bus power
- Preconditioning trickle charge
- Guaranteed to operate down to 2.65V after start-up
- Ambient temperature range: -40°C to +85°C
- AEC-Q100 qualified

Applications

- Automotive systems
- eCall systems
- Backup battery systems

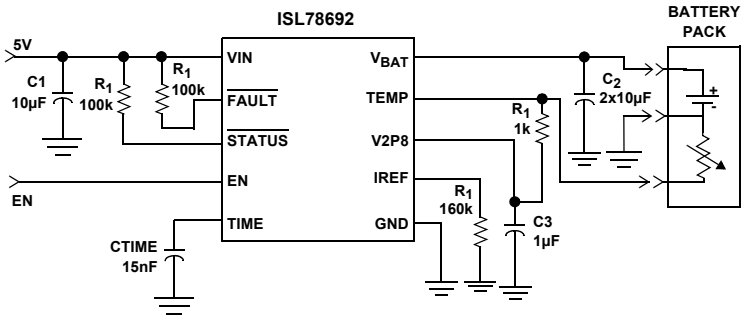


FIGURE 1. TYPICAL APPLICATION

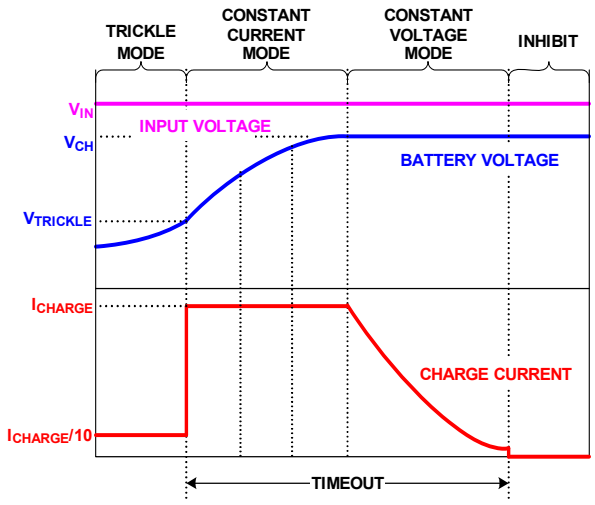


FIGURE 2. TYPICAL CHARGE CURVES USING A CONSTANT VOLTAGE ADAPTER

Block Diagram

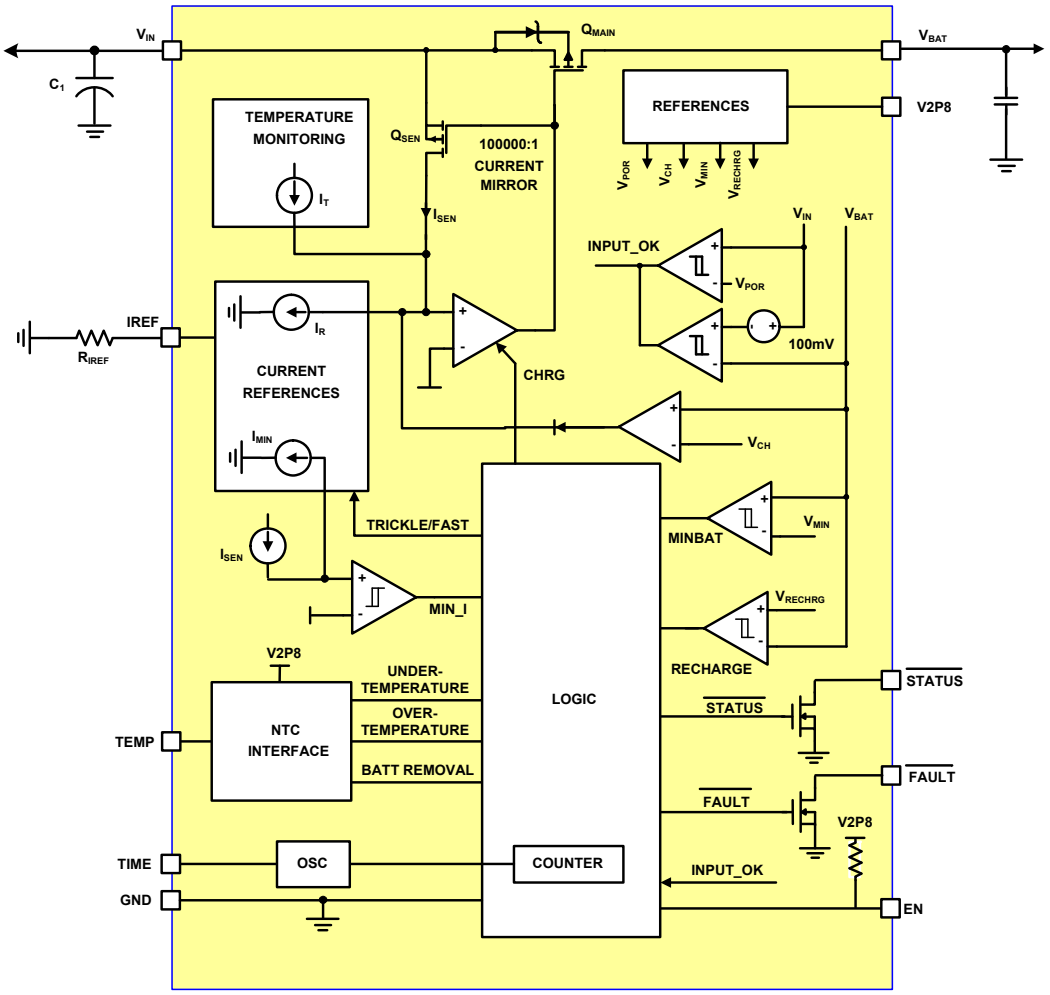


TABLE 1. KEY DIFFERENCES BETWEEN FAMILY OF PARTS

PART NUMBER	OUTPUT VOLTAGE (V)	RECHARGE THRESHOLD (V)	TRICKLE CHARGE THRESHOLD (V)
ISL78692	4.1	3.9	2.8
ISL78693	3.65	3.25	2.6

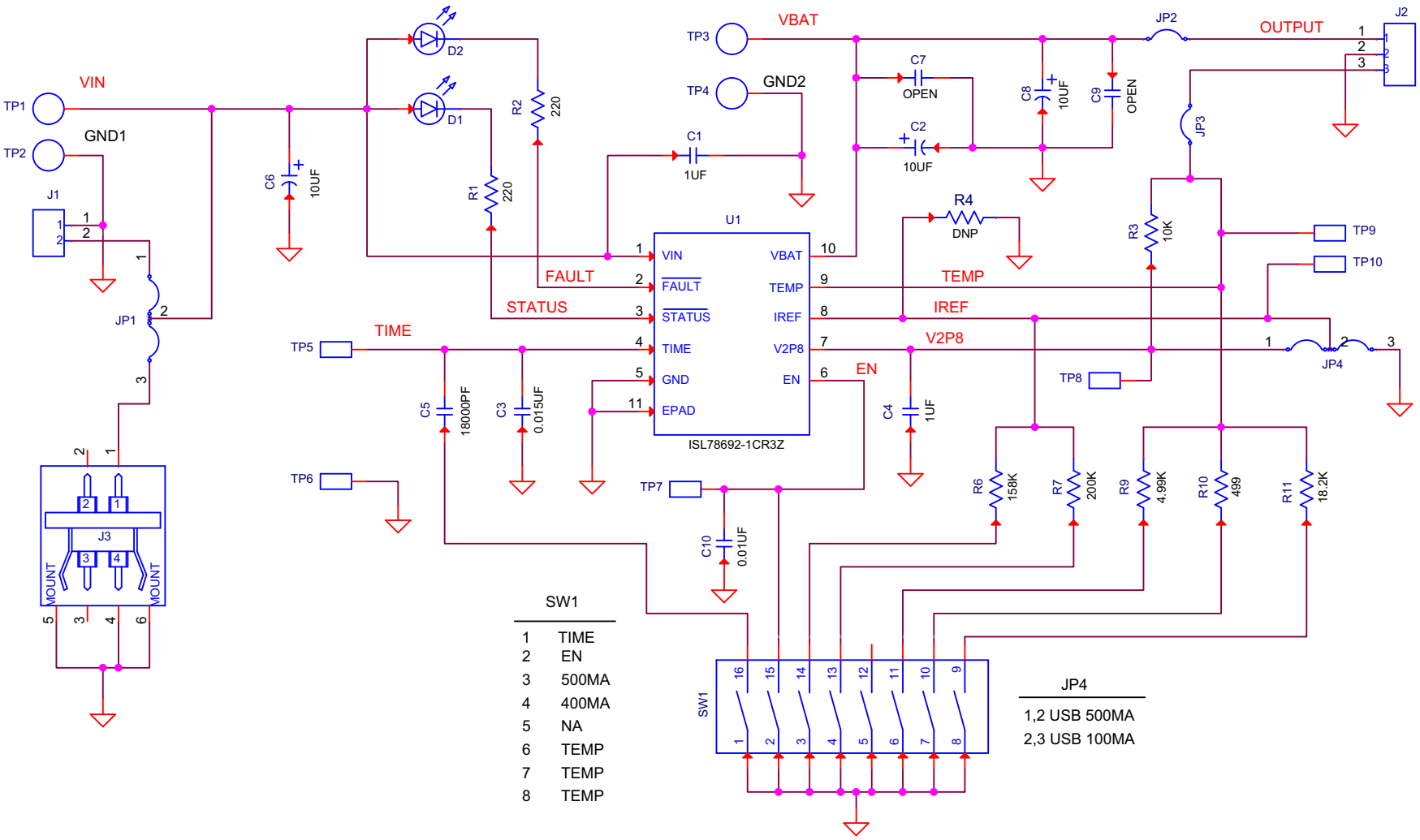
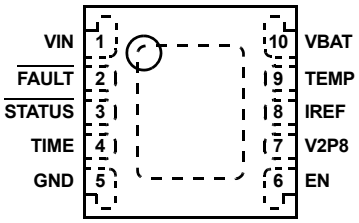


FIGURE 3. ISL78692EVAL1Z SCHEMATIC

Pin Configuration

ISL78692
(10 LD 3x3 DFN)
TOP VIEW



Pin Descriptions

PIN #	PIN NAME	DESCRIPTION
1	VIN	VIN is the input power source.
2	$\overline{\text{FAULT}}$	$\overline{\text{FAULT}}$ is an open-drain output indicating fault status. This pin is pulled to LOW under any fault conditions.
3	$\overline{\text{STATUS}}$	$\overline{\text{STATUS}}$ is an open-drain output indicating charging and inhibit states. The $\overline{\text{STATUS}}$ pin is pulled LOW when the charger is charging a battery.
4	TIME	The TIME pin determines the oscillation period by connecting a timing capacitor between this pin and GND. The oscillator also provides a time reference for the charger.
5	GND	GND is the connection to system ground.
6	EN	EN is the enable logic input. Connect the EN pin to LOW to disable the charger or leave it floating to enable the charger.
7	V2P8	The V2P8 is a 2.8V reference voltage output. The 2.8V is present when VIN is above 3.4V typical. If VIN falls below 2.4V typical the V2P8 output will be at 0V.
8	IREF	This is the programming input for the constant charging current.
9	TEMP	TEMP is the input for an external NTC thermistor. The TEMP pin is also used for battery removal detection.
10	VBAT	VBAT is the connection to the battery.
	EPAD	The metal slug on the bottom surface of the package is floating. Tie to system GND.

Ordering Information

PART NUMBER (Notes 1, 2, 3)	PART MARKING	TEMP RANGE (°C)	PACKAGE (Pb-Free)	PKG DWG
ISL78692-1CR3Z	8692	-40 to +85	10 Ld 3x3 DFN	L10.3x3
ISL78692EVAL1Z	Evaluation Board for the 3x3 DFN Package Part			

NOTE:

1. Add “-T” suffix for 6k unit or “-T7A” suffix for 250 unit tape and reel options. Refer to TB347 for details on reel specifications.
2. These Intersil Pb-free plastic packaged products employ special Pb-free material sets, molding compounds/die attach materials, and 100% matte tin plate plus anneal (e3 termination finish, which is RoHS compliant and compatible with both SnPb and Pb-free soldering operations). Intersil Pb-free products are MSL These Intersil Pb-free plastic packaged products employ special Pb-free material sets, molding compounds/die attach materials, and 100% matte tin plate plus classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.
3. For Moisture Sensitivity Level (MSL), please see device information page for ISL78692. For more information on MSL, see Technical Brief TB363.

Absolute Maximum Ratings

Supply Voltage (VIN) . . . . . -0.3V to 7.0V
Output Pin Voltage (VBAT) . . . . . -0.3V to 5.5V
Output Pin Voltage (V2P8) . . . . . -0.3V to 3.2V
Signal Input Voltage (EN, TIME, IREF, TEMP) . . . . . -0.3V to 3.2V
Output Pin Voltage ($\overline{\text{STATUS}}$, $\overline{\text{FAULT}}$) . . . . . -0.3V to 7.0V
Charge Current 1.6A
ESD Rating:
Human Body Model (Tested per AEC-Q100-002) 4kV
Charge Device Model (Tested per AEC-Q100-011) 1.25kV
Latch-up (Per JESD78D; Class 2, Level A, AEC-Q100-004) 100mA

Thermal Information

Thermal Resistance (Typical)	θ_{JA} (°C/W)	θ_{JC} (°C/W)
3x3 DFN Package (Notes 4, 5)	46	4

Maximum Junction Temperature . . . . . +150°C
Maximum Storage Temperature Range . . . . . -65°C to +150°C
Pb-Free Reflow Profile . . . . . see TB493

Recommended Operating Conditions

Ambient Temperature Range . . . . . -40°C to +85°C
Supply Voltage, VIN . . . . . 4.3V to 5.5V

CAUTION: Do not operate at or near the maximum ratings listed for extended periods of time. Exposure to such conditions may adversely impact product reliability and result in failures not covered by warranty.

NOTES:

4. θ_{JA} is measured in free air with the component mounted on a high effective thermal conductivity test board with "direct attach" features. See Tech Brief TB379.
5. θ_{JC}, "case temperature" location is at the center of the exposed metal pad on the package underside. See Tech Brief TB379.

Electrical Specifications

Typical values are tested at V_{IN} = 5V and at an Ambient Temperature of +25°C. Unless otherwise noted. **Boldface limits apply across the operating temperature range, -40°C to +85°C and V_{IN} range of 4.3V to 5.5V** (see Note 6).

PARAMETER	SYMBOL	TEST CONDITIONS	MIN (Note 6)	TYP	MAX (Note 6)	UNITS
POWER-ON RESET						
Rising V_{IN} Threshold			**3.0**	3.4	**4.0**	V
Falling V_{IN} Threshold			**2.11**	2.4	**2.65**	V
STANDBY CURRENT						
VBAT Pin Leakage	I_{VBLKG}	V_{BAT} = 5.5V, V_{IN} = 0V, EN = 0.8V		0.7	**3.0**	µA
VIN Pin Standby Current	I_{INSBY}	V_{BAT} OPEN, V_{IN} = 5.0V, EN = 0.8V		30	**200**	µA
VIN Pin Quiescent Current	I_Q	V_{BAT} OPEN, V_{IN} = 5.5V, EN FLOAT		1		mA
VOLTAGE REGULATION						
Output Voltage	V_{CH}	V_{BAT} OPEN	**4.015**	4.10	**4.185**	V
Dropout Voltage	V_{DO}	V_{BAT} = 3.7V, I_{IN} = 500mA		270	**450**	mV
CHARGE CURRENT						
Constant Charge Current (Note 8)	I_{CHARGE}	R_{IREF} = 160kΩ, V_{BAT} = 3.7V	**430**	500	**570**	mA
Trickle Charge Current	$I_{TRICKLE}$	R_{IREF} = 160kΩ, V_{BAT} = 2.4V		55		mA
Constant Charge Current (Note 8)	I_{CHARGE}	IREF pin voltage > 1.2V, V_{BAT} = 3.7V	**390**	450	**540**	mA
Trickle Charge Current	$I_{TRICKLE}$	IREF pin voltage > 1.2V, V_{BAT} = 2.4V		45		mA
Constant Charge Current (Note 8)	I_{CHARGE}	IREF pin voltage < 0.4V, V_{BAT} = 3.7V	**65**	80	**104**	mA
Trickle Charge Current	$I_{TRICKLE}$	IREF pin voltage < 0.4V, V_{BAT} = 2.4V		10		mA
End-of-Charge Current	I_{EOC}		**35**	60	**100**	mA
RECHARGE THRESHOLD						
Recharge Voltage Falling Threshold	V_{RECHRG}		**3.7**	3.9	**4.05**	V
TRICKLE CHARGE THRESHOLD						
Trickle Charge Threshold Voltage	$V_{TRICKLE}$		**2.7**	2.8	**3.0**	V

Electrical Specifications

Typical values are tested at V_{IN} = 5V and at an Ambient Temperature of +25°C. Unless otherwise noted. **Boldface limits apply across the operating temperature range, -40°C to +85°C and V_{IN} range of 4.3V to 5.5V** (see Note 6).

PARAMETER	SYMBOL	TEST CONDITIONS	MIN (Note 6)	TYP	MAX (Note 6)	UNITS
TEMPERATURE MONITORING						
Low Temperature Threshold	V_{TMIN}	V2P8 = 3.0V	**1.45**	1.51	**1.57**	V
High Temperature Threshold	V_{TMAX}	V2P8 = 3.0V	**0.36**	0.38	**0.4**	V
Battery Removal Threshold (Note 7)	V_{RMV}	V2P8 = 3.0V, Voltage on temperature	**2.1**	2.25	**3.0**	V
Charge Current Foldback Threshold	T_{FOLD}	Junction temperature	**85**	100	**125**	°C
Current Foldback Gain (Note 7)	G_{FOLD}			100		mA/°C
OSCILLATOR						
Oscillation Period	t_{OSC}	C_{TIME} = 15nF	**2.2**	3.0	**3.6**	ms
LOGIC INPUT AND OUTPUT						
EN Input Low					**0.8**	V
IREF Input High			**1.2**			V
IREF Input Low					**0.4**	V
$\overline{STATUS}$/ $\overline{FAULT}$ Sink Current		Pin voltage = 0.8V	**5**	11		mA

NOTES:

6. The Parameters with MIN and/or MAX limits are 100% tested at +25°C, unless otherwise specified. Temperature limits established by characterization and are not production tested.
7. This parameter is not tested in production.
8. Measured using pulse load.

Typical Operating Performance

The test conditions for the Typical Operating Performance are: V_{IN} = 5V, T_A = +25°C, R_{IREF} = 160kΩ, V_{BAT} = 3.7V, Unless Otherwise Noted.

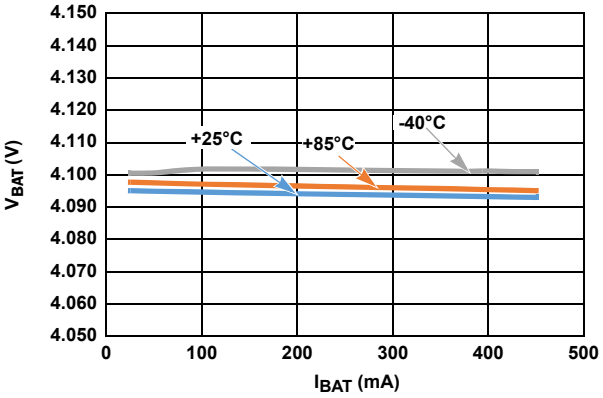


FIGURE 4. VOLTAGE REGULATION vs CHARGE CURRENT

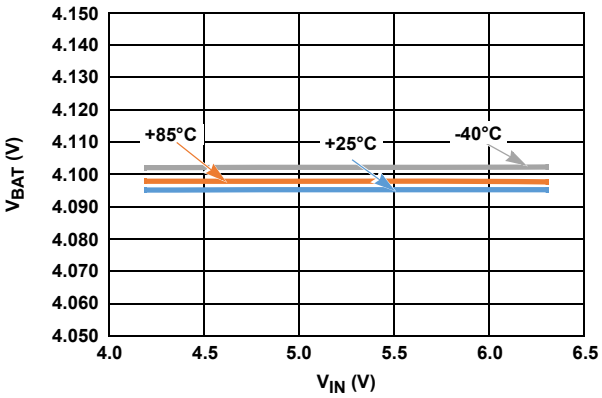


FIGURE 5. NO LOAD VOLTAGE vs TEMPERATURE

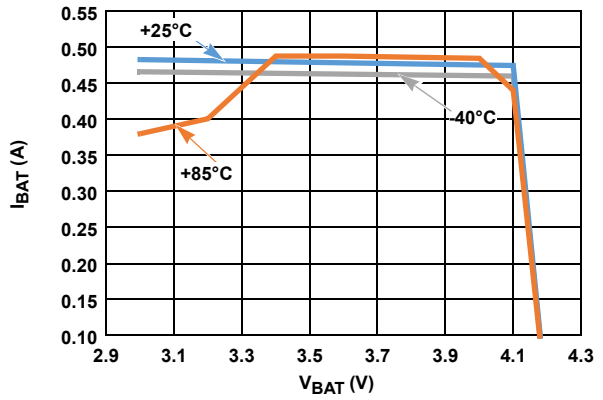


FIGURE 6. CHARGE CURRENT vs OUTPUT VOLTAGE, R_{IREF} = 158k

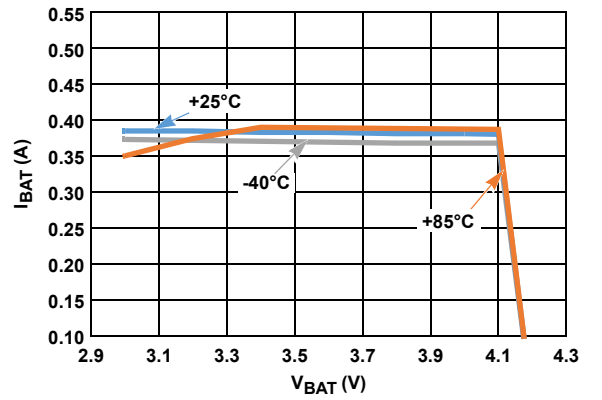


FIGURE 7. CHARGE CURRENT vs OUTPUT VOLTAGE, R_{IREF} = 200k

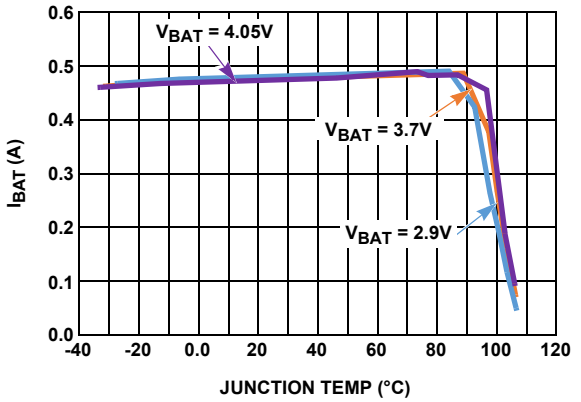


FIGURE 8. CHARGE CURRENT vs JUNCTION TEMPERATURE, R_{IREF} = 158k

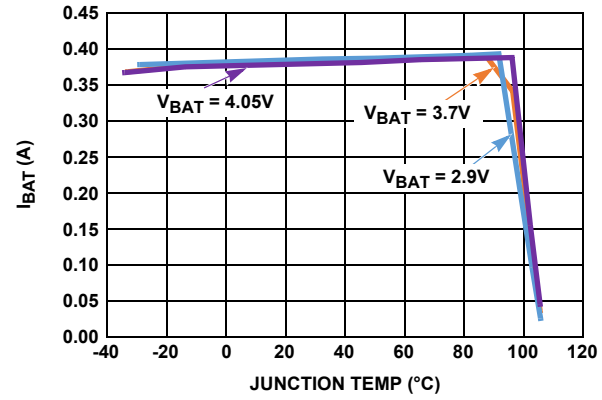


FIGURE 9. CHARGE CURRENT vs JUNCTION TEMPERATURE, R_{IREF} = 200k

Typical Operating Performance

The test conditions for the Typical Operating Performance are: V_{IN} = 5V, T_A = +25°C, R_{IREF} = 160kΩ, V_{BAT} = 3.7V, Unless Otherwise Noted. **(Continued)**

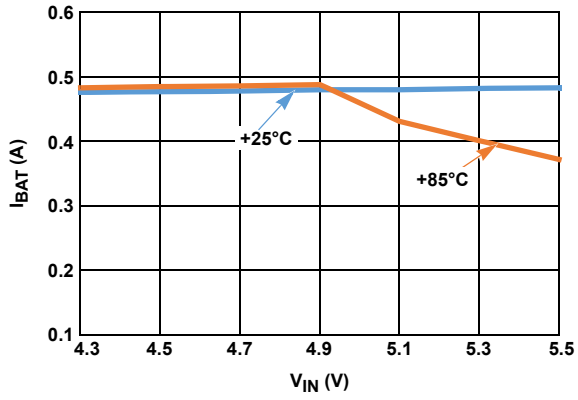


FIGURE 10. CHARGE CURRENT vs INPUT VOLTAGE, V_{BAT} = 3V, R_{IREF} = 158k

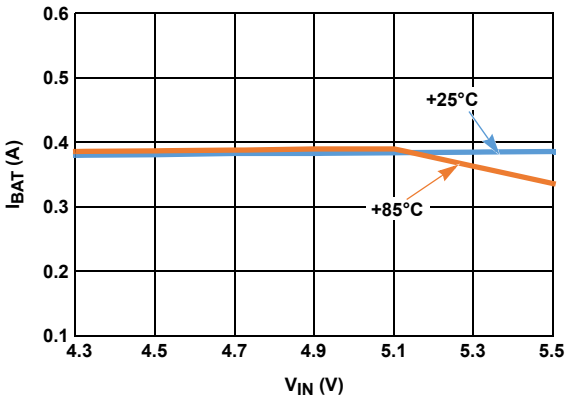


FIGURE 11. CHARGE CURRENT vs INPUT VOLTAGE, V_{BAT} = 3V, R_{IREF} = 200k

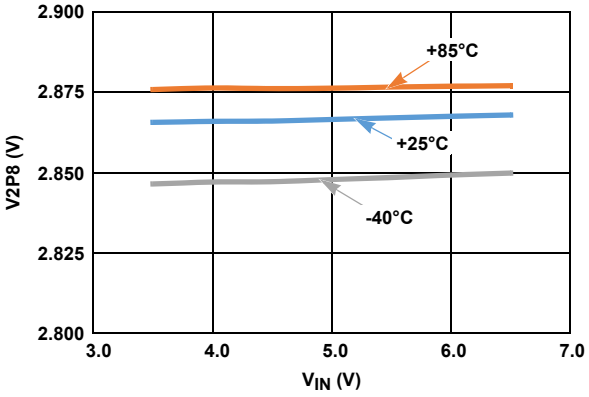


FIGURE 12. V2P8 OUTPUT vs INPUT VOLTAGE AT NO LOAD

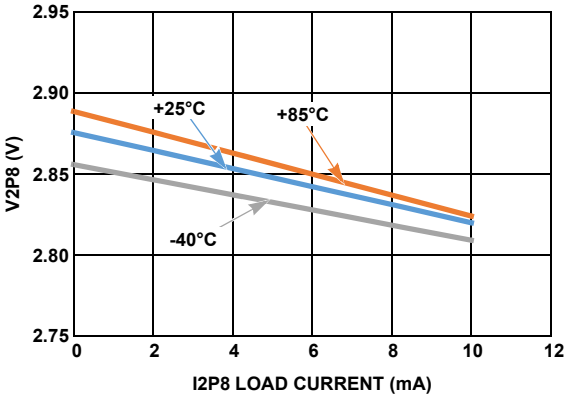


FIGURE 13. V2P8 OUTPUT vs LOAD CURRENT

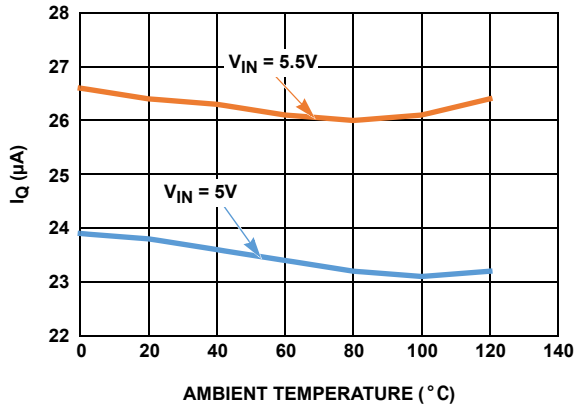


FIGURE 14. INPUT QUIESCENT CURRENT vs TEMPERATURE

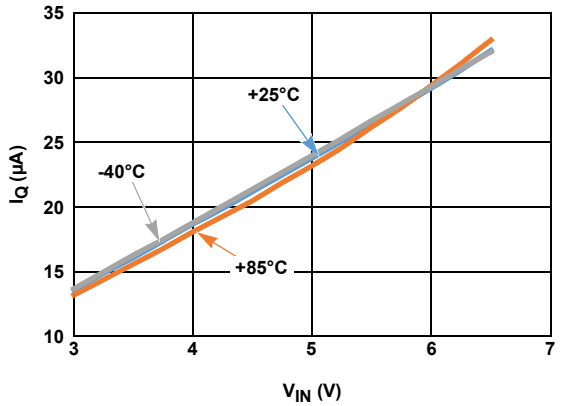


FIGURE 15. INPUT QUIESCENT CURRENT vs INPUT VOLTAGE, SHUTDOWN

Typical Operating Performance

The test conditions for the Typical Operating Performance are: V_{IN} = 5V, T_A = +25°C, R_{IREF} = 160kΩ, V_{BAT} = 3.7V, Unless Otherwise Noted. **(Continued)**

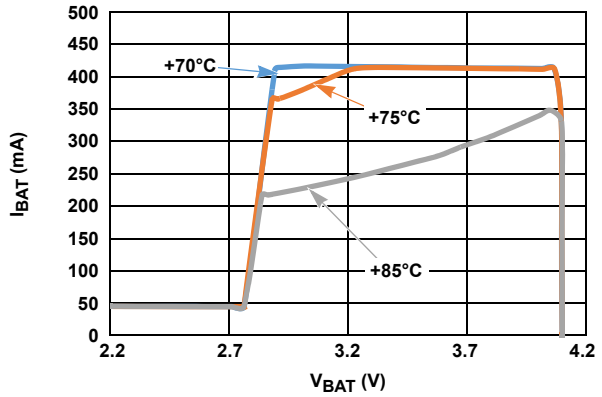


FIGURE 16. V_{BAT} vs I_{BAT} vs AMBIENT TEMPERATURE, R_{IREF} = 200k, V_{IN} = 5.5V, AIR FLOW = 0 LFM, MEASURED ON THE ISL78692EVAL1Z BOARD

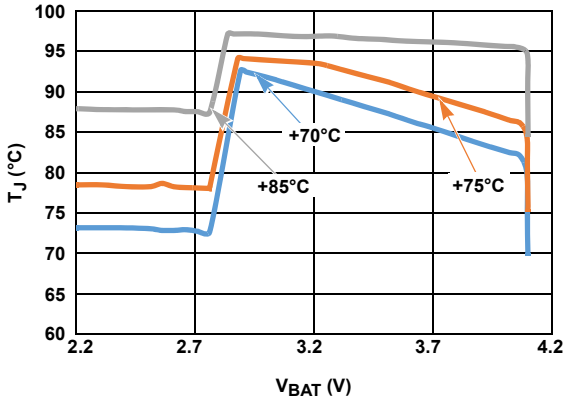


FIGURE 17. JUNCTION TEMPERATURE vs V_{BAT} vs AMBIENT TEMPERATURE, R_{IREF} = 200k, V_{IN} = 5.5V, AIR FLOW = 0 LFM, MEASURED ON THE ISL78692EVAL1Z BOARD

Theory of Operation

The ISL78692 is an integrated charger for single-cell Lithium chemistry batteries. The ISL78692 functions as a traditional linear charger when powered with a voltage source adapter. When powered with a current-limited adapter, the charger minimizes the thermal dissipation commonly seen in traditional linear chargers.

As a linear charger, the ISL78692 charges a battery in the popular constant current (CC) and constant voltage (CV) profile. The constant charge current I_{REF} is programmable up to 1A with an external resistor or a logic input. The charge voltage V_{CH} has 1% accuracy over the entire recommended operating condition range. The charger preconditions the battery with a 10% typical of the programmed current at the beginning of a charge cycle until the battery voltage is verified to be above the minimum fast charge voltage, $V_{TRICKLE}$. This low current preconditioning charge mode is named trickle mode. The verification takes 15 cycles of an internal oscillator whose period is programmable with a timing capacitor on the time pin. A thermal-foldback feature protects the device from the thermal concern typically seen in linear chargers. The charger reduces the charge current automatically as the IC internal temperature rises above +100°C to prevent further temperature rise. The thermal-foldback feature guarantees safe operation when the printed circuit board (PCB) is space limited for thermal dissipation.

A TEMP pin monitors the battery temperature to ensure a safe charging temperature range. The temperature range is programmable with an external negative temperature coefficient (NTC) thermistor. The TEMP pin is also used to detect the removal of the battery.

The charger offers a safety timer for setting the fast charge time (TIMEOUT) limit to prevent charging a dead battery for an extensively long time. The trickle mode is limited to 1/8 of TIMEOUT.

The charger automatically recharges the battery when the battery voltage drops below a recharge threshold of 3.9V (typ).

When the input supply is not present, the ISL78692 draws less than 1µA current from the battery.

Three indication pins are available from the charger to indicate the charge status. The V2P8 outputs a 2.8VDC voltage when the input voltage is above the power-on reset (POR) level and can be used as the power-present indication. This pin is capable of sourcing a 2mA current, so it can also be used to bias external circuits. The $\overline{\text{STATUS}}$ pin is an open-drain logic output that turns LOW at the beginning of a charge cycle until the end-of-charge (EOC) condition is qualified. The EOC condition is when the battery voltage rises above the recharge threshold and the charge current falls below a preset of a tenth of the programmed charge current. Once the EOC condition is qualified, the $\overline{\text{STATUS}}$ output rises to HIGH and is latched. The latch is released at the beginning of a charge or recharge cycle. The open-drain $\overline{\text{FAULT}}$ pin turns low when any fault conditions occur. The fault conditions include the external battery temperature fault, a charge time fault, or the battery removal.

Figure 18 shows the typical charge curves in a traditional linear charger powered with a constant voltage adapter. From top to bottom, the curves represent the constant input voltage, the battery voltage, the charge current and the power dissipation in the charger. The power dissipation P_{CH} is given by Equation 1:

$$P_{CH} = (V_{IN}-V_{BAT}) \cdot I_{CHARGE} \quad \text{(EQ. 1)}$$

where I_{CHARGE} is the charge current. The maximum power dissipation occurs during the beginning of the CC mode. The maximum power the IC is capable of dissipating is dependent on the thermal impedance of the printed circuit board (PCB). Figure 18 shows (with dotted lines) two cases that the charge currents are limited by the maximum power dissipation capability due to the thermal foldback.

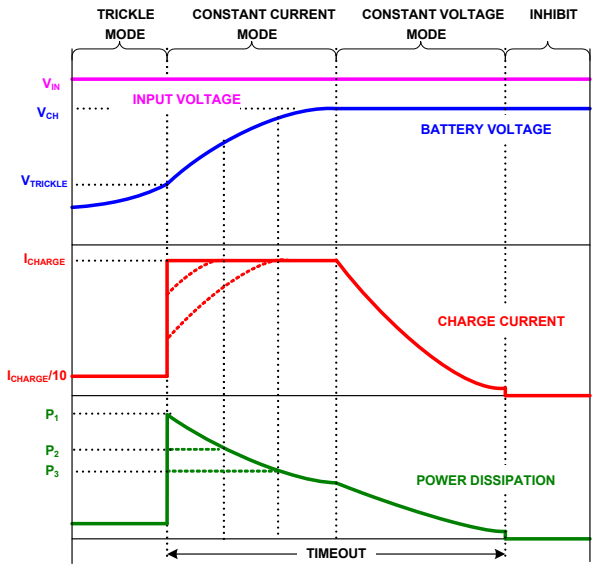


FIGURE 18. TYPICAL CHARGE CURVES USING A CONSTANT VOLTAGE ADAPTER

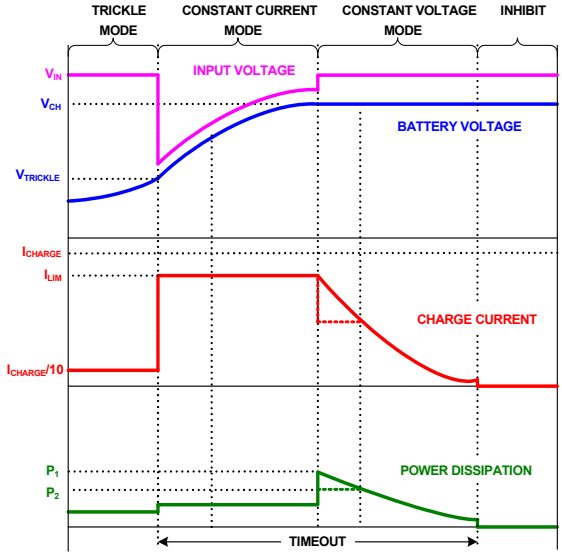


FIGURE 19. TYPICAL CHARGE CURVES USING A CURRENT-LIMITED ADAPTER

When using a current-limited adapter, the thermal situation in the ISL78692 is totally different. Figures 19 shows the typical charge curves when a current-limited adapter is employed. The operation requires the I_{REF} to be programmed higher than the limited current I_{LIM} of the adapter. The key difference of the charger operating under such conditions occurs during the CC mode.

The "Block Diagram" on page 2 aids in understanding the operation. The current loop consists of the current amplifier CA and the sense MOSFET (Q_{SEN}). The current reference I_R is programmed by the IREF pin. The current amplifier CA regulates the gate of the sense MOSFET (Q_{SEN}) that the sensed current I_{SEN} matches the reference current I_R. The main MOSFET Q_{MAIN} and the sense MOSFET (Q_{SEN}) form a current mirror with a ratio of 100,000:1, which the output charge current is 100,000 times I_R. In the CC mode, the current loop tries to increase the charge current by enhancing the sense MOSFET (Q_{SEN}), which the sensed current matches the reference current. On the other hand, the adapter current is limited, the actual output current will never meet what is required by the current reference. As a result, the current error amplifier CA, keeps enhancing the Q_{SEN} as well as the main MOSFET Q_{MAIN} until they are fully turned on. Therefore, the main MOSFET becomes a power switch instead of a linear regulation device. The power dissipation in the CC mode becomes Equation 2:

$$P_{CH} = r_{DS(ON)} \cdot I_{CHARGE}^2 \quad \text{(EQ. 2)}$$

where $r_{DS(ON)}$ is the resistance when the main MOSFET is fully turned on. This power is typically much less than the peak power in the traditional linear mode.

The worst power dissipation when using a current-limited adapter typically occurs at the beginning of the CV mode, as shown in Figure 19.

Equation 1 applies during the CV mode. When using a very small PCB whose thermal impedance is relatively large, it is possible that the internal temperature can still reach the thermal foldback threshold. In that case, the IC is thermally protected by lowering the charge current, as shown with the dotted lines in the charge current and power curves. Appropriate design of the adapter can further reduce the peak power dissipation of the ISL78692. See "Applications Information" for more information.

Figure 20 illustrates the typical signal waveforms for the linear charger from the power-up to a recharge cycle. More detailed information is given in the following.

Applications Information

Power on Reset (POR)

The ISL78692 resets itself as the input voltage rises above the POR rising threshold. The V2P8 pin outputs a 2.8V voltage, the internal oscillator starts to oscillate, the internal timer is reset, and the charger begins to charge the battery. The two indication pins, $\overline{STATUS}$ and $\overline{FAULT}$, indicate a LOW and a HIGH logic signal respectively. Figure 20 illustrates the start-up of the charger between t_0 to t_2.

The ISL78692 has a typical rising POR threshold of 3.4V and a falling POR threshold of 2.4V. The 2.4V falling threshold guarantees charger operation with a current-limited adapter to minimize the thermal dissipation.

Charge Cycle

A charge cycle consists of three charge modes: trickle mode, constant current (CC) mode and constant voltage (CV) mode. The charge cycle always starts with the trickle mode until the battery voltage stays above $V_{TRICKLE}$ (2.8V typical) for 15 consecutive cycles of the internal oscillator. If the battery voltage drops below $V_{TRICKLE}$ during the 15 cycles, the 15-cycle counter is reset and the charger stays in the trickle mode. The charger moves to the CC mode after verifying the battery voltage. As the battery pack terminal voltage rises to the final charge voltage V_{CH}, the CV mode begins. The terminal voltage is regulated at the constant V_{CH} in the CV mode and the charge current starts to reduce towards zero.

After the charge current drops below $I_{(EOC)}$ programmed to 1/10 of I_{REF}; see "End-of-Charge (EOC) Current" on page 12 for more detail), the ISL78692 indicates the end-of-charge (EOC) with the $\overline{STATUS}$ pin. The charging actually does not terminate until the internal timer completes its length of TIMEOUT in order to bring the battery to its full capacity. Signals in a charge cycle are illustrated in Figure 20 between points t_2 to t_5.

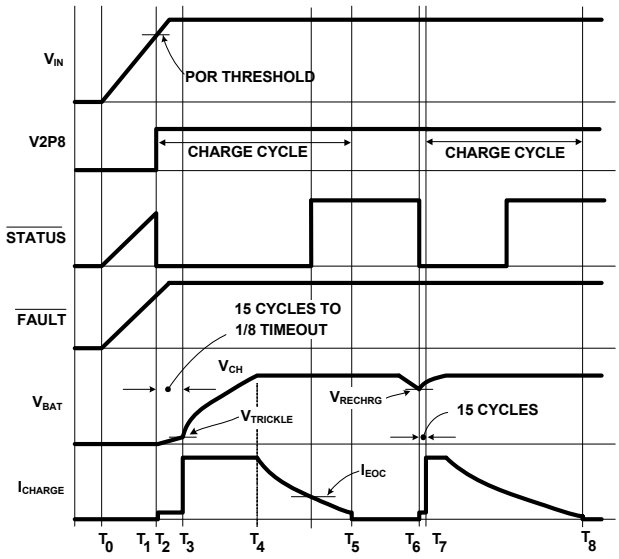


FIGURE 20. OPERATION WAVEFORMS

The following events initiate a new charge cycle:

- POR
- A new battery being inserted (detected by TEMP pin)
- The battery voltage drops below a recharge threshold after completing a charge cycle
- Recovery from an battery over-temperature fault
- Or, the EN pin is toggled from GND to floating
- Further description of these events are given later in this datasheet

Recharge

After a charge cycle completes, charging is prohibited until the battery voltage drops to a recharge threshold, V_{RECHRG} of 3.9V (TYP), (see "Electrical Specifications" on page 5"). Then a new charge cycle starts at point t_6 and ends at point t_8, as shown in Figure 20. The safety timer is reset at t_6.

Internal Oscillator

The internal oscillator establishes a timing reference. The oscillation period is programmable with an external timing capacitor, C_{TIME}, as shown in Figure 1. The oscillator charges the timing capacitor to 1.5V and then discharges it to 0.5V in one period, both with 10µA current. The period t_{OSC} is given by Equation 3:

$$t_{OSC} = 0.2 \bullet 10^6 \bullet C_{TIME} \quad \text{(seconds)} \qquad \text{(EQ. 3)}$$

A 1nF capacitor results in a 0.2ms oscillation period. The accuracy of the period is mainly dependent on the accuracy of the capacitance and the internal current source.

Total Charge Time

The total charge time for the CC mode and CV mode is limited to a length of TIMEOUT. A 22-stage binary counter increments each oscillation period of the internal oscillator to set the TIMEOUT. The TIMEOUT can be calculated in Equation 4:

$$TIMEOUT = 2^{22} \bullet \left(\frac{t_{OSC(SEC)}}{60}\right) = 14 \bullet \frac{C_{TIME}}{1nF}(minutes) \qquad \text{(EQ. 4)}$$

A 1nF capacitor leads to 14 minutes of TIMEOUT. For example, a 15nF capacitor sets the TIMEOUT to be 3.5 hours. The charger has to reach the end-of-charge condition before the TIMEOUT, otherwise, a TIMEOUT fault is issued. The TIMEOUT fault latches up the charge and the $\overline{FAULT}$ pin goes low. There are two ways to release such a latch-up either to recycle the input power, or toggle the EN pin to disable the charger and then enable it again.

The trickle charge mode has a time limit of 1/8 TIMEOUT. If the battery voltage does not reach $V_{TRICKLE}$ within this limit, a TIMEOUT fault is issued and the charger latches off. The charger stays in trickle mode for at least 15 cycles of the internal oscillator and, at most, 1/8 of TIMEOUT, as shown in Figure 20.

Charge Current Programming

The charge current is programmed by the IREF pin. There are three ways to program the charge current:

1. Driving the IREF pin above 1.2V
2. Driving the IREF pin below 0.4V,
3. Or using the R_{IREF} as shown in "TYPICAL APPLICATION" on page 1.

The voltage of IREF is regulated to a 0.8V reference voltage when not driven by any external source. The charging current during the constant current mode is 100,000 times that of the current in the R_{IREF} resistor. Hence, depending on how IREF pin is used, the charge current is given by Equation 5:

$$I_{REF} = \begin{cases} 500mA & V_{IREF} > 1.2V \\ \frac{0.8V}{R_{IREF}} \times 10^5 (A) & R_{IREF} \\ 80mA & V_{IREF} < 0.4V \end{cases} \qquad \text{(EQ. 5)}$$

The internal reference voltage at the IREF pin is capable of sourcing less than 100µA current. When pulling down the IREF pin with a logic circuit, the logic circuit must be able to sink at least 100µA current. For design purposes, a designer should assume a tolerance of ±20% when computing the minimum and maximum charge current from Equation 5.

When the adapter is current limited, it is recommended that the reference current be programmed to at least 30% higher than the adapter current limit (which equals the charge current). In addition, the charge current should be at least 350mA, which the voltage difference between the VIN and the VBAT pins is higher than 100mV. The 100mV is the offset voltage of the input/output voltage comparator shown in "Block Diagram" on page 2.

End-of-Charge (EOC) Current

The end-of-charge current I_{EOC} sets the level at which the charger starts to indicate the end of the charge with the $\overline{STATUS}$ pin, as shown in Figure 20. The charger actually does not terminate charging until the end of the TIMEOUT, as described in "Total Charge Time" on page 11. The I_{EOC} is set to 60mA (typ) internal to the device by tying the I_{EOC} node to V2P8.

Charge Current Thermal Foldback

Overheating is always a concern in a linear charger. The maximum power dissipation usually occurs at the beginning of a charge cycle when the battery voltage is at its minimum but the charge current is at its maximum. The charge current thermal foldback function in the ISL78692 frees users from the overheating concern.

Figure 21 shows the current signals at the summing node of the current error amplifier in "Block Diagram" on page 2. I_R is the reference and I_T is the current from the temperature monitoring block. The I_T has no impact on the charge current until the internal temperature reaches approximately +100°C (+85°C Min) then I_T rises at a rate of 1µA/°C. When I_T rises, the current control loop forces the sensed current I_{SEN} to reduce at the same rate. As a mirrored current, the charge current is 100,000 times that of the sensed current and reduces at a rate of 100mA/°C. For a charger with the constant charge current set at 1A, the charge current is reduced to zero when the internal temperature rises to +110°C. The actual charge current settles between +100°C to +110°C.

The charge current should not drop below I_{EOC} because of the thermal foldback. For some extreme cases (if that does happen) the charger does not indicate end-of-charge unless the battery voltage is already above the recharge threshold.

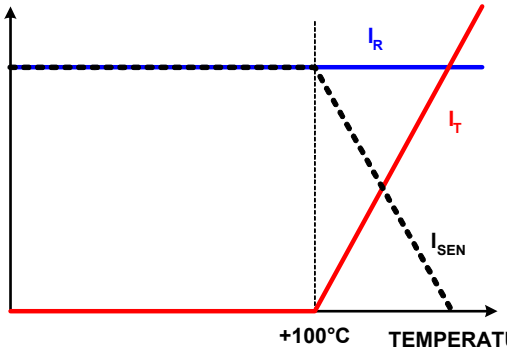


FIGURE 21. CURRENT SIGNALS AT THE AMPLIFIER AC INPUT

2.8V Bias Voltage

The ISL78692 provides a 2.8V voltage for biasing the internal control and logic circuit. This voltage is also available for external circuits such as the NTC thermistor circuit. The maximum allowed external load is 2mA.

NTC Thermistor

The ISL78692 uses two comparators (CP2 and CP3) to form a window comparator, as shown in Figure 23. When the TEMP pin voltage is "out of the window," determined by the V_{TMIN} and V_{TMAX}, the ISL78692 stops charging and indicates a fault condition. When the temperature returns to the set range, the charger re-starts a charge cycle. The two MOSFETs, Q1 and Q2, produce hysteresis for both upper and lower thresholds. The temperature window is shown in Figure 22.

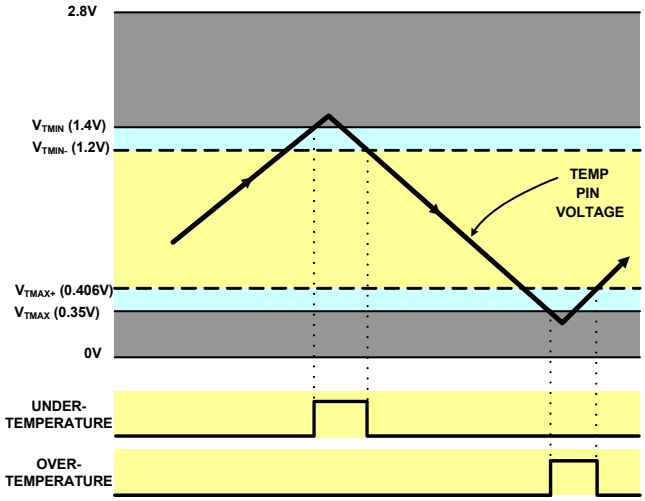


FIGURE 22. CRITICAL VOLTAGE LEVELS FOR TEMP PIN

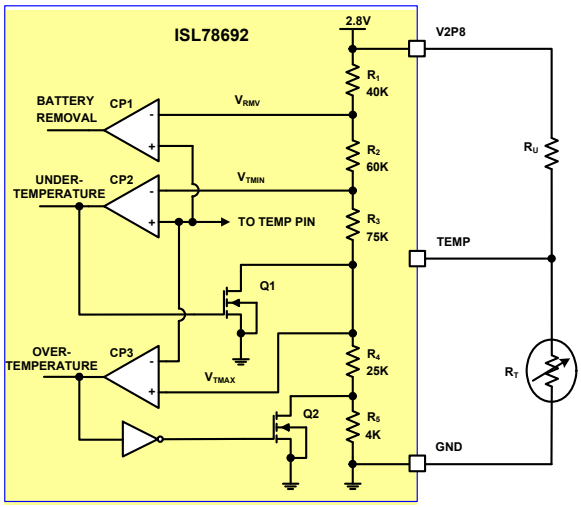


FIGURE 23. THE INTERNAL AND EXTERNAL CIRCUIT FOR THE NTC INTERFACE

As the TEMP pin voltage rises from low and exceeds the 1.4V threshold, the under-temperature signal rises and does not clear until the TEMP pin voltage falls below the 1.2V falling threshold. Similarly, the over-temperature signal is given when the TEMP pin voltage falls below the 0.35V threshold and does not clear until the voltage rises above 0.406V. The actual accuracy of the 2.8V is **not important** because all the thresholds and the TEMP pin voltage are ratios determined by the resistor dividers, as shown in Figure 23.

The NTC thermistor is required to have a resistance ratio of 7:1 at the low and the high temperature limits, that is given by Equation 6:

$$\frac{R_{COLD}}{R_{HOT}} = 7 \quad \text{(EQ. 6)}$$

This is because at the low temperature limit, the TEMP pin voltage is 1.4V, which is 1/2 of the 2.8V bias, as shown in Equation 7:

$$R_{COLD} = R_U \quad \text{(EQ. 7)}$$

where R_U is the pull-up resistor as shown in Figure 23. On the other hand, at the high temperature limit the TEMP pin voltage is 0.35V, 1/8 of the 2.8V bias (see Equation 8):

$$R_{HOT} = \frac{R_U}{7} \quad \text{(EQ. 8)}$$

Various NTC thermistors are available for this application. Table 2 shows the resistance ratio and the negative temperature coefficient of the curve-1 NTC thermistor from Vishay at various temperatures. The resistance at +3°C is approximately seven times the resistance at +47°C, which is shown in Equation 9:

$$\frac{R_{3°C}}{R_{47°C}} = 7 \quad \text{(EQ. 9)}$$

If the low temperature limit is +3°C, and the high temperature limit is around +47°C. The pull-up resistor RU can be chosen to be the resistance measured at +3°C.

TABLE 2. RESISTANCE RATIO OF VISHAY'S CURVE-1 NTC

TEMPERATURE (°C)	$R_T/R_{25°C}$	NTC (%/°C)
0	3.266	5.1
3	2.806	5.1
5	2.540	5.0
25	1.000	4.4
45	0.4368	4.0
47	0.4041	3.9
50	0.3602	3.9

The temperature hysteresis will now be estimated in the low and high temperatures. At the low temperature, the hysteresis is approximately estimated in Equation 10:

$$T_{hysLOW} \approx \frac{1.4V - 1.2V}{1.4V \cdot 0.051} \approx 3 \quad (°C) \quad \text{(EQ. 10)}$$

where 0.051 is the NTC at +3°C. Similarly, the high temperature hysteresis is estimated in Equation 11:

$$T_{hysHIGH} \approx \frac{0.406V - 0.35V}{0.35V \cdot 0.039} \approx 4 \quad (°C) \quad \text{(EQ. 11)}$$

where the 0.039 is the NTC at +47°C.

For applications that do not need to monitor the battery temperature, the NTC thermistor can be replaced with a regular resistor of a half value of the pull-up resistor R_U. Another option is to connect the TEMP pin to the IREF pin that has a 0.8V output. With such connection, the IREF pin can no longer be programmed with logic inputs. In this condition no pull-up is allowed for the TEMP pin.

Battery Removal Detection

The ISL78692 assumes that the thermistor is co-packed with the battery and is removed together with the battery. When the charger senses a TEMP pin voltage that is 2.1V or higher, it assumes that the battery is removed. The battery removal detection circuit is also shown in Figure 23. When a battery is removed, a $\overline{\text{FAULT}}$ signal is indicated and charging is halted. When a battery is inserted again, a new charge cycle starts.

Indications

The ISL78692 has three indications: the input presence, the charge status, and the fault indication. The input presence is indicated by the V2P8 pin while the other two indications are presented by the $\overline{\text{STATUS}}$ pin and $\overline{\text{FAULT}}$ pin respectively. Figure 24 shows the V2P8 pin voltage vs the input voltage. Table 3 summarizes the other two pins.

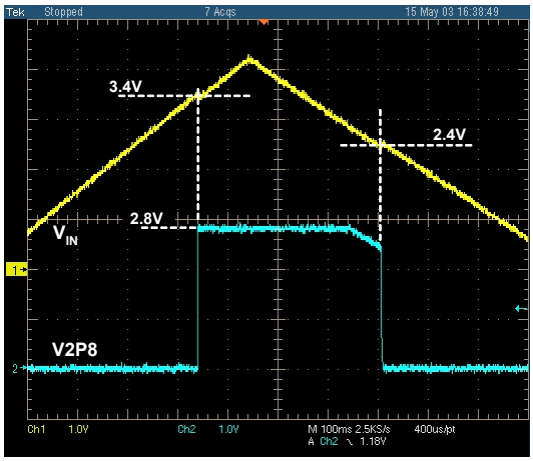


FIGURE 24. THE V2P8 PIN OUTPUT vs THE INPUT VOLTAGE AT THE VIN PIN. VERTICAL: 1V/DIV, HORIZONTAL: 100ms/DIV

TABLE 3. STATUS INDICATIONS

$\overline{\text{FAULT}}$	$\overline{\text{STATUS}}$	INDICATION
High	High	Charge completed with no fault (Inhibit) or Standby
High	Low	Charging in one of the three modes
Low	High	Fault

*Both outputs are pulled up with external resistors.

Shutdown

The ISL78692 can be shut down by pulling the EN pin to ground. When shut down, the charger draws typically less than 30µA current from the input power and the 2.8V output at the V2P8 pin is also turned off. The EN pin has to be driven with an open-drain or open-collector logic output. The EN pin is internally biased, so the pin should be floated to turn the device ON once the charger is enabled. To turn OFF the device an open drain/open collector can be used to pull the pin to its low level.

Input and Output Capacitor Selection

The use of a 10µF Tantalum type TCA106M016R0200 or Ceramic type C3216X7RC1106KT000N or equivalent is recommended for the input. When used as a charger, the output capacitor should be 2x10µF Tantalum type AVX TCJA106M016R0200 or equivalent. The device partially relies on the ESR (equivalent series resistance) of the output capacitor for the loop stability. If there is a need to use ceramic capacitors for device output, it is recommended to use a 220mΩ, 0.25W resistor, in series with the VBAT pin followed by 2x10µF, 16V, X7R ceramic capacitor C3216X7RC1106KT000N or equivalent for an I_{BAT} = 0.5A (see Figure 25).

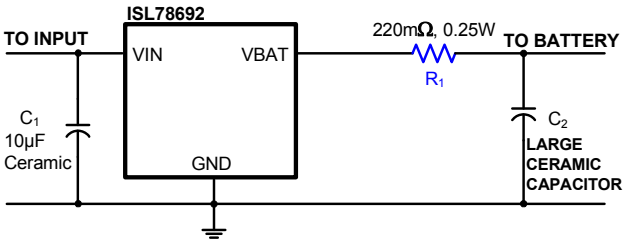


FIGURE 25. INSERTING R_1 TO IMPROVE THE STABILITY OF APPLICATIONS WITH LARGE CERAMIC CAPACITOR USED AT THE OUTPUT

Current-Limited Adapter

Figure 26 shows the ideal current voltage characteristics of a current-limited adapter. The V_{NL} is the no-load adapter output voltage and V_{FL} is the full load voltage at the current limit I_{LIM}. Before its output current reaches the limit I_{LIM}, the adapter presents the characteristics of a voltage source. The slope, r_O, represents the output resistance of the voltage supply. For a well regulated supply, the output resistance can be very small, but some adapters naturally have a certain amount of output resistance.

The adapter is equivalent to a current source when running in the constant current region. Being a current source, its output voltage is dependent on the load, which in this case, is the charger and the battery. As the battery is being charged, the adapter output rises from a lower voltage in the current voltage characteristics curve, such as point A, to higher voltage until reaching the breaking point B, as shown in Figure 26.

The adapter is equivalent to a voltage source with output resistance when running in the constant voltage region; because of this characteristic. As the charge current drops, the adapter output moves from point B to point C, shown in Figure 26.

The battery pack can be approximated as an ideal cell with a lumped-sum resistance in series, also shown in Figure 26. The ISL78692 charger sits between the adapter and the battery.

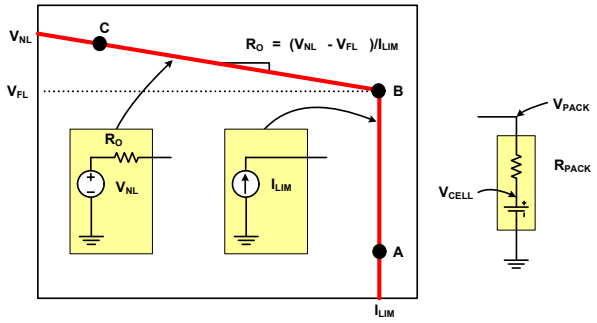


FIGURE 26. THE IDEAL I-V CHARACTERISTICS OF A CURRENT LIMITED POWER SUPPLY

Working with Current-Limited Power Supply

As described earlier, the ISL78692 minimizes the thermal dissipation when running off a current-limited AC adapter, as shown in Figure 19. The thermal dissipation can be further reduced when the adapter is properly designed. The following demonstrates that the thermal dissipation can be minimized if the adapter output reaches the full-load output voltage (point B in Figure 26) before the battery pack voltage reaches the final charge voltage (4.1V). The assumptions for the following discussion are: the adapter current limit = 500mA, the battery pack equivalent resistance = 200mΩ, and the charger ON-resistance is 350mΩ.

When charging in the constant current region, the pass element in the charger is fully turned on. The charger is equivalent to the ON-resistance of the internal P-Channel MOSFET. The entire charging system is equivalent to the circuit shown in Figure 27A. The charge current is the constant current limit I_{LIM}, and the adapter output voltage can be easily found out as calculated in Equation 12:

$$V_{Adapter} = I_{LIM} \bullet r_{DS(ON)} V_{PACK} \quad \text{(EQ. 12)}$$

where V_{PACK} is the battery pack voltage. The power dissipation in the charger is given in Equation 2, where $I_{CHARGE} = I_{LIM}$.

A critical condition of the adapter design is that the adapter output reaches point B in Figure 26 at the same time as the battery pack voltage reaches the final charge voltage (4.1V), that is given by Equation 13:

$$V_{Critical} = I_{LIM} \cdot r_{DSON} + V_{CH} \quad \text{(EQ. 13)}$$

For example, if the final charge voltage is 4.1V, the $r_{DS(ON)}$ is 350mΩ, and the current limit I_{LIM} is 500mA, the critical adapter full-load voltage is 4.275V.

When the above condition is true, the charger enters the constant voltage mode simultaneously as the adapter exits the current limit mode. The equivalent charging system is shown in Figure 27C. Since the charge current drops at a higher rate in the constant voltage mode than the increase rate of the adapter voltage, the power dissipation decreases as the charge current decreases. Therefore, the worst case thermal dissipation occurs in the constant current charge mode. Figure 27A shows the I-V curves of the adapter output, the battery pack voltage and the cell voltage during the charge. The 5.9V no-load voltage is just an example value higher than the full-load voltage. The cell voltage

4.05V uses the assumption that the pack resistance is 200mΩ. Figure 28A illustrates the adapter voltage, battery pack voltage, the charge current and the power dissipation in the charger respectively in the time domain.

If the battery pack voltage reaches 4.1V before the adapter reaches point B in Figure 26, a voltage step is expected at the adapter output when the pack voltage reaches the final charge voltage. As a result, the charger power dissipation is also expected to have a step rise. This case is shown in Figure 19 as well as Figure 29C. Under this condition, the worst case thermal dissipation in the charger happens when the charger enters the constant voltage mode.

If the adapter voltage reaches the full-load voltage before the pack voltage reaches 4.1V, the charger will experience the resistance-limit situation. In this situation, the ON-resistance of the charger is in series with the adapter output resistance. The equivalent circuit for the resistance-limit region is shown in Figure 27B. Eventually, the battery pack voltage will reach 4.1V because the adapter no-load voltage is higher than 4.1V, then Figure 27C becomes the equivalent circuit until charging ends. In this case, the worst-case thermal dissipation also occurs in the constant current charge mode. Figure 28B shows the I-V curves of the adapter output, the battery pack voltage and the cell voltage for the case VFL = 4V. In the case, the full-load voltage is lower than the final charge voltage (4.1V), but the charger is still able to fully charge the battery as long as the no-load voltage is above 4.1V. Figure 28B illustrates the adapter voltage, battery pack voltage, the charge current and the power dissipation in the charger respectively in the time domain.

Based on the previous discussion, the worst-case power dissipation occurs during the constant current charge mode if the adapter full-load voltage is lower than the critical voltage given in Equation 13. Even if that is not true, the power dissipation is still much less than the power dissipation in the traditional linear charger. Figures 26 and 27 are scope-captured waveforms to demonstrate the operation with a current-limited adapter.

The waveforms in Figure 26 are the adapter output voltage (1V/div), the battery voltage (1V/div), and the charge current (200mA/div) respectively. The time scale is 1ks/div. The adapter current is limited to 600mA and the charge current is programmed to 1A. Note that the voltage difference is only approximately 200mV and the adapter voltage tracks the battery voltage in the CC mode. Figure 26 also shows the resistance limit mode before entering the CV mode.

Figure 27 shows the actual captured waveforms depicted in Figure 29C. The constant charge current is 750mA. A step in the adapter voltage during the transition from CC mode to CV mode is demonstrated.

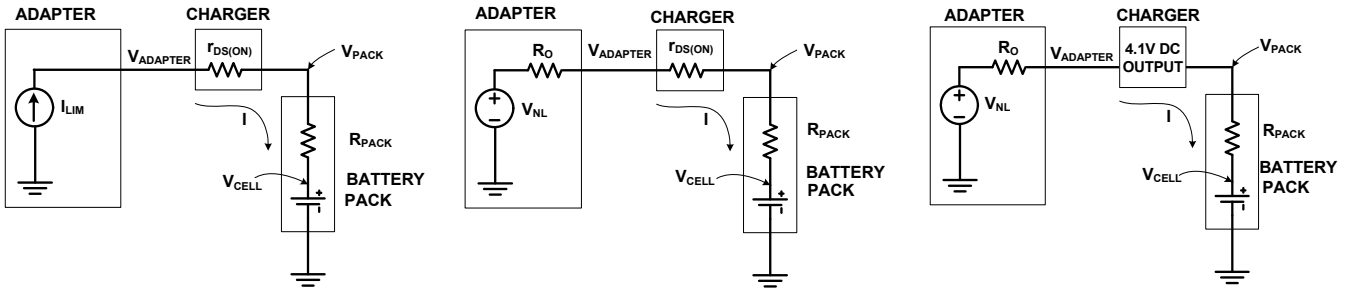


FIGURE 27A. THE EQUIVALENT CIRCUIT IN THE CONSTANT CURRENT REGION

FIGURE 27B. THE EQUIVALENT CIRCUIT IN THE RESISTANCE-LIMIT REGION

FIGURE 27C. THE EQUIVALENT CIRCUIT WHEN THE PACK VOLTAGE REACHES THE FINAL CHARGE VOLTAGE

FIGURE 27. THE EQUIVALENT CIRCUIT OF THE CHARGING SYSTEM WORKING WITH CURRENT LIMITED ADAPTERS

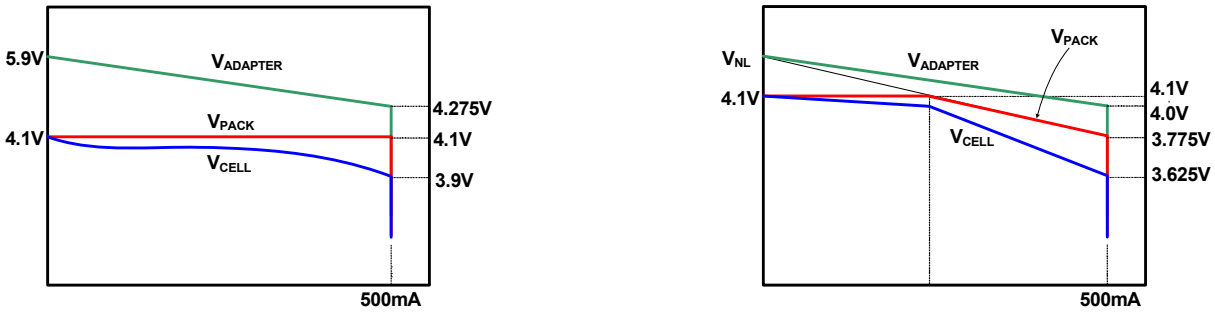


FIGURE 28A.

FIGURE 28B.

FIGURE 28. THE I-V CHARACTERISTICS OF THE CHARGER WITH DIFFERENT CURRENT LIMITED POWER SUPPLIES

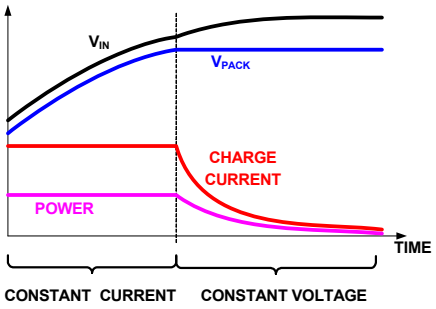


FIGURE 29A.

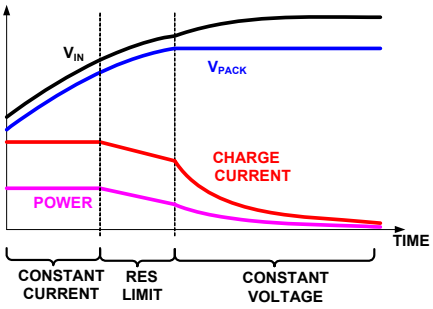


FIGURE 29B.

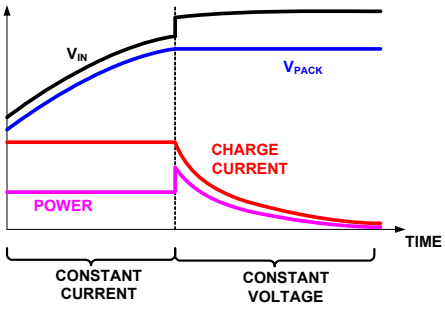


FIGURE 29C.

FIGURE 29. THE OPERATING CURVES WITH THREE DIFFERENT CURRENT LIMITED POWER SUPPLIES

IREF Programming Using Current-Limited Adapter

The ISL78692 has 20% tolerance for the charge current. Typically, the current-limited adapter also has 10% tolerance. In order to guarantee proper operation, it is recommended that the nominal charge current be programmed **at least 30% higher** than the nominal current limit of the adapter.

Board Layout Recommendations

The ISL78692 internal thermal foldback function limits the charge current when the internal temperature reaches approximately +100°C. In order to maximize the current capability, it is very important that the exposed pad under the package is properly soldered to the board and is connected to other layers through thermal vias. More thermal vias and more copper attached to the exposed pad usually result in better thermal performance. On the other hand, the number of vias is limited by the size of the pad. The 3x3 DFN package allows 9 vias be placed in three rows. Since the pins on the 3x3 DFN package are on only two sides, as much top layer copper as possible should be connected to the exposed pad to minimize the thermal impedance. Refer to UG001, "ISL78692EVAL1Z Evaluation Board User Guide"for layout example.

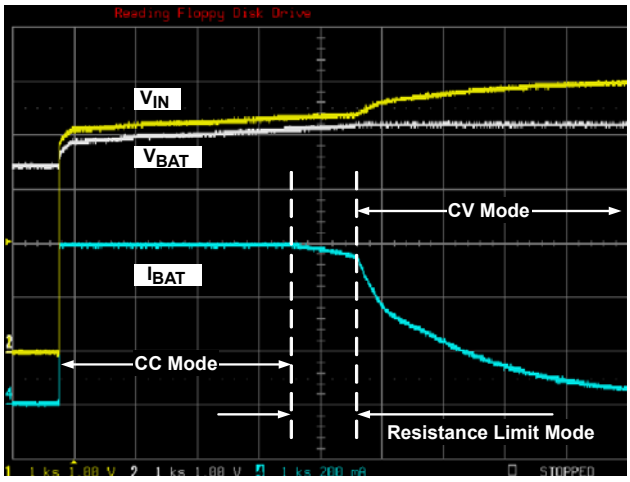


FIGURE 30. SCOPE WAVEFORMS SHOWING THE THREE MODE

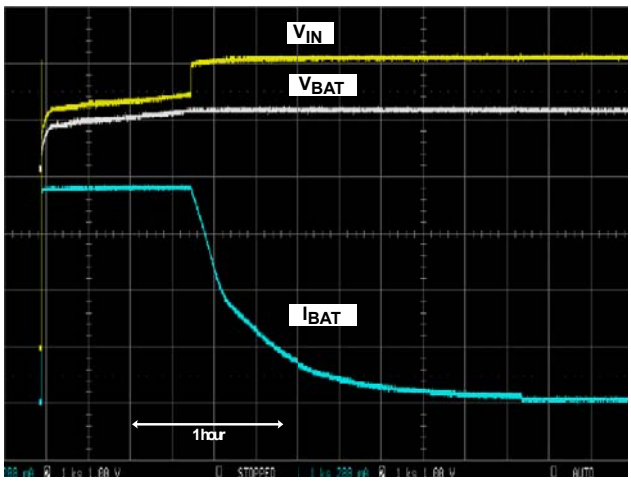


FIGURE 31. SCOPE WAVEFORMS SHOWING THE CASE THAT THE FULL-LOAD POWER SUPPLY VOLTAGE IS HIGHER THAN THE CRITICAL VOLTAGE

Revision History

The revision history provided is for informational purposes only and is believed to be accurate, but not warranted. Please visit our website to make sure you have the latest revision.

DATE	REVISION	CHANGE
March 29, 2017	FN8692.1	Added Key Differences Between Family of parts on page 2. Ordering Information table on page 4: added to Note 1, -T7A and tape and reel quantities. Updated POD L10.3x3 on page 18 from rev 10 to rev 11. Changes since rev 10: Tiebar Note 4 updated From: Tiebar shown (if present) is a non-functional feature. To: Tiebar shown (if present) is a non-functional feature and may be located on any of the 4 sides (or ends).
September 10, 2014	FN8692.0	Initial Release.

About Intersil

Intersil Corporation is a leading provider of innovative power management and precision analog solutions. The company's products address some of the largest markets within the industrial and infrastructure, mobile computing and high-end consumer markets.

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For a listing of definitions and abbreviations of common terms used in our documents, visit: www.intersil.com/glossary.

You may report errors or suggestions for improving this datasheet by visiting www.intersil.com/ask.

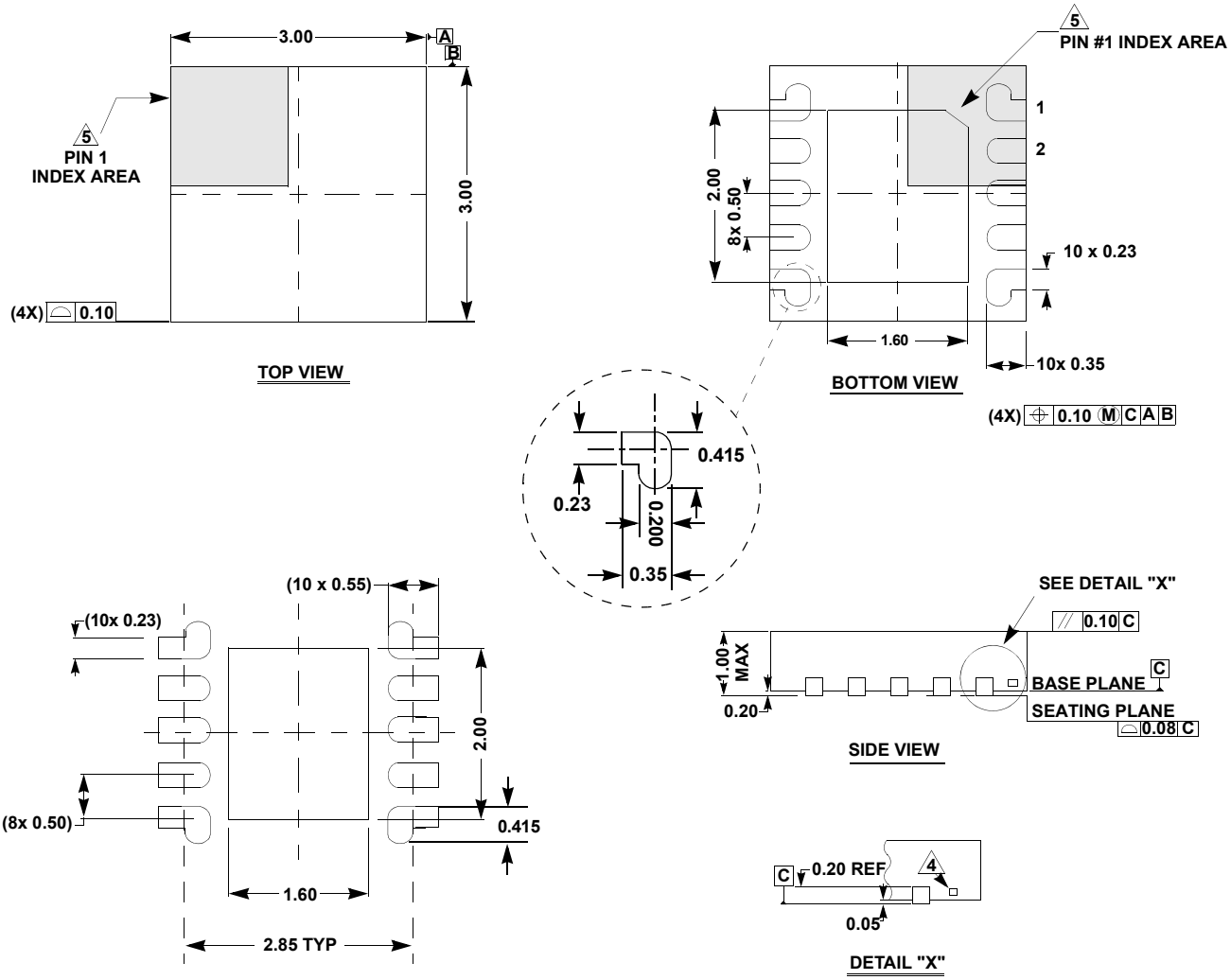
Reliability reports are also available from our website at www.intersil.com/support

Package Outline Drawing

For the most recent package outline drawing, see L10.3x3.

L10.3x3

10 LEAD DUAL FLAT PACKAGE (DFN)
Rev 11, 3/15



NOTES:

1. Dimensions are in millimeters.
   Dimensions in ( ) for Reference Only.
2. Dimensioning and tolerancing conform to ASME Y14.5m-1994.
3. Unless otherwise specified, tolerance : Decimal ± 0.05
4. Tiebar shown (if present) is a non-functional feature and may be located on any of the 4 sides (or ends).
5. The configuration of the pin #1 identifier is optional, but must be located within the zone indicated. The pin #1 identifier may be either a mold or mark feature.